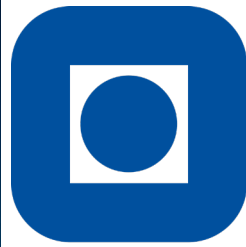




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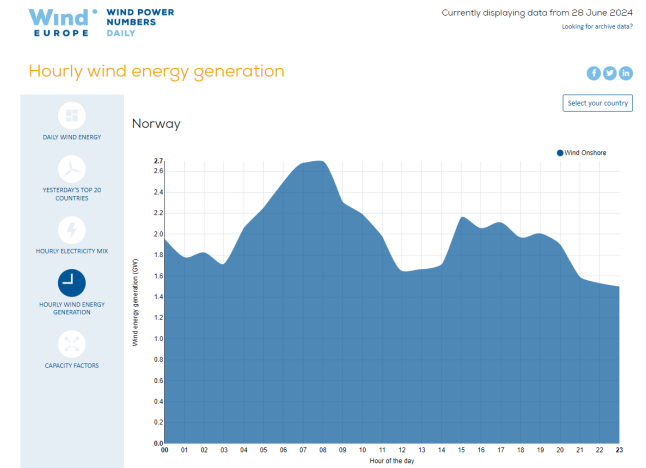
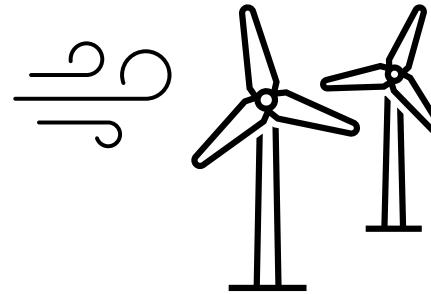
Control of Multi-Stack PEM Water Electrolyzer Systems: From Optimal Operation to Control Design

NPCW 2026 – 18.08.2026

Marius Fredriksen (NTNU) and Johannes Jäschke (NTNU)

PEM Electrolyzers Face a Dynamic Environment

- Hydrogen to store and transport green energy
- Fluctuating energy output from renewable sources such as wind and solar
- Volatile Energy prices
- Hydrogen demand from downstream consumers



fortum

Electricity contracts and services

Customer benefits

Customer support



Spot prices

Daily Yearly

< 9 Apr 2026 >

• 12.45 - 13.00

7,17 c/kWh

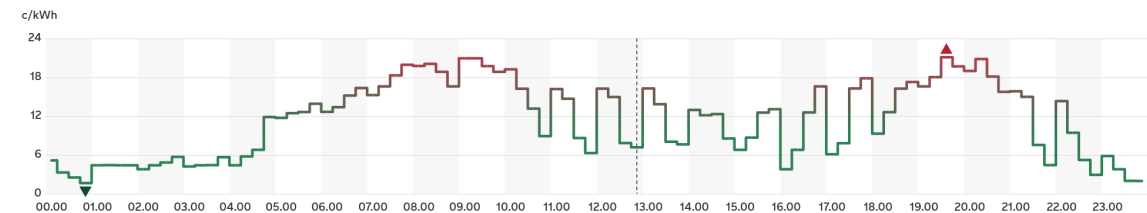
▼ Lowest price ▲ Highest price

1,65 c/kWh

00.45 - 01.00

21,06 c/kWh

19.30 - 19.45



Daily average price 11,37 c/kWh

1.

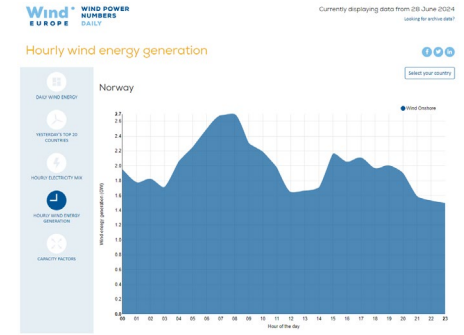
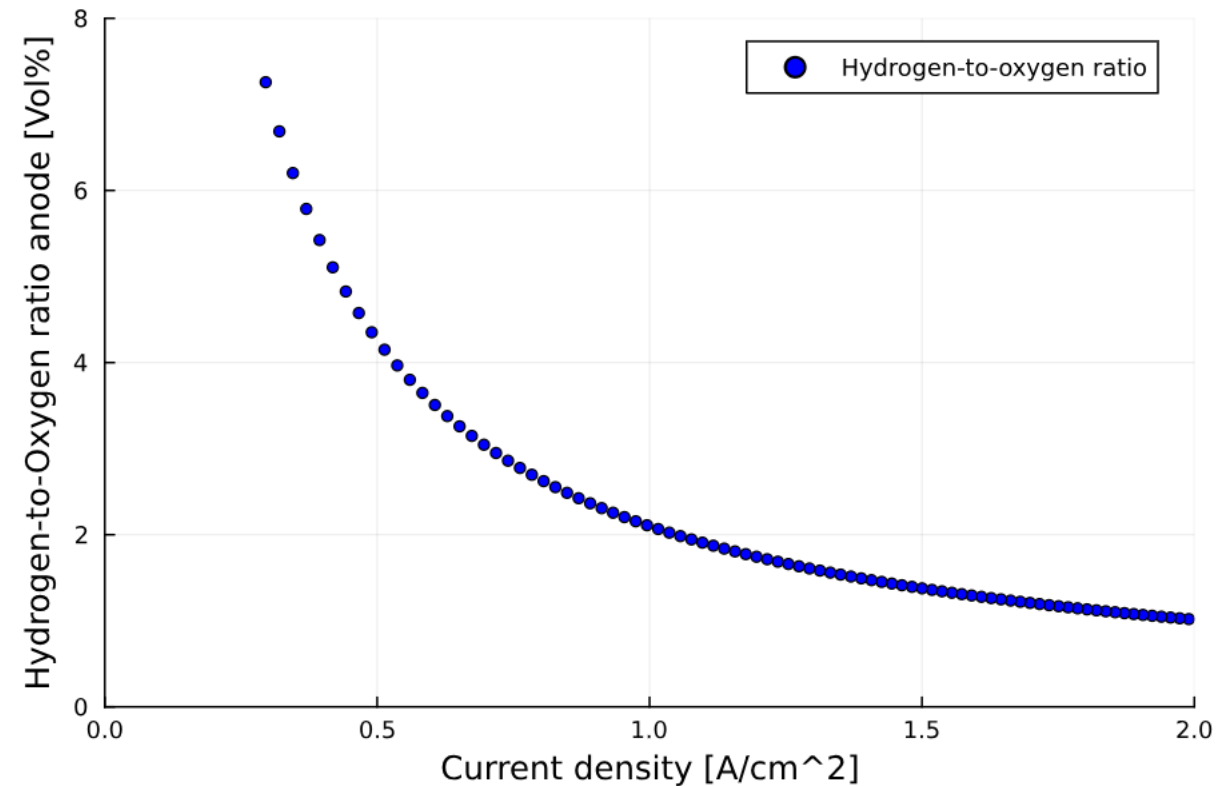


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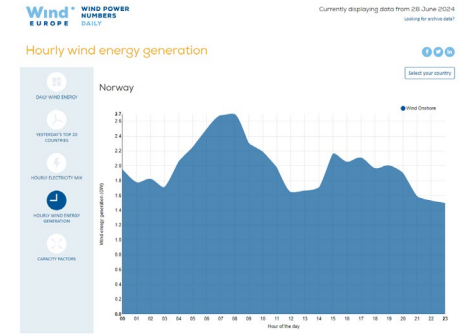


Fluctuations and Safety

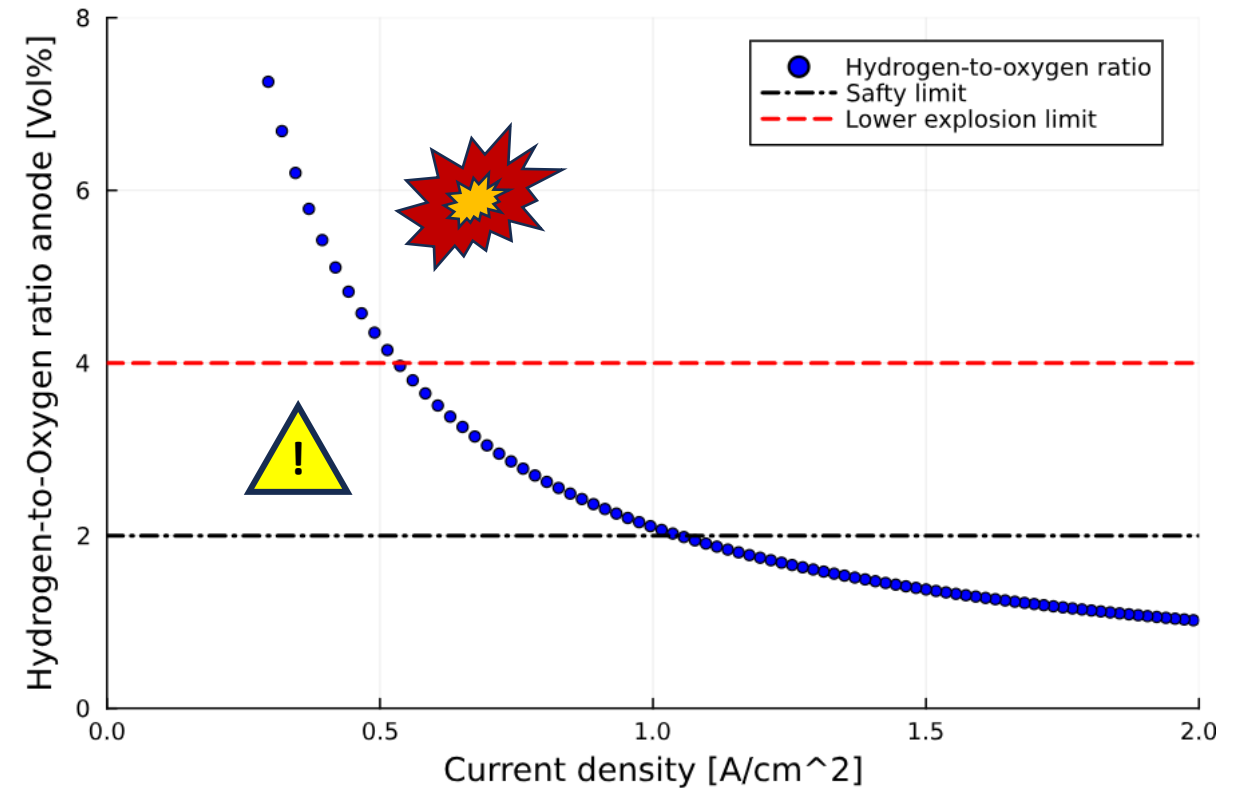
- The Hydrogen-to-Oxygen ratio (HTO) is closely related to the power input
 - At low power, we have lower current density
 - At low current densities, we have high HTO



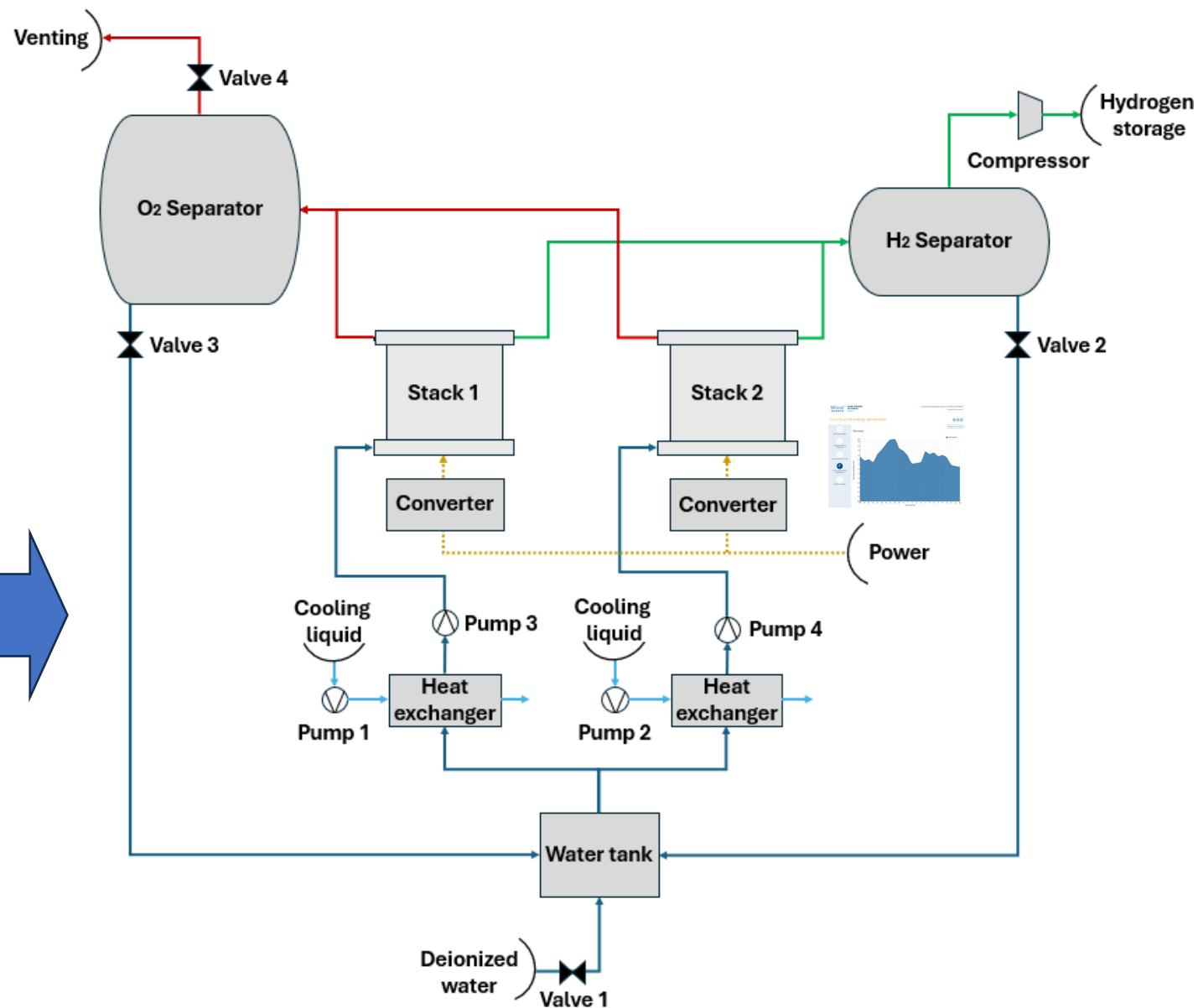
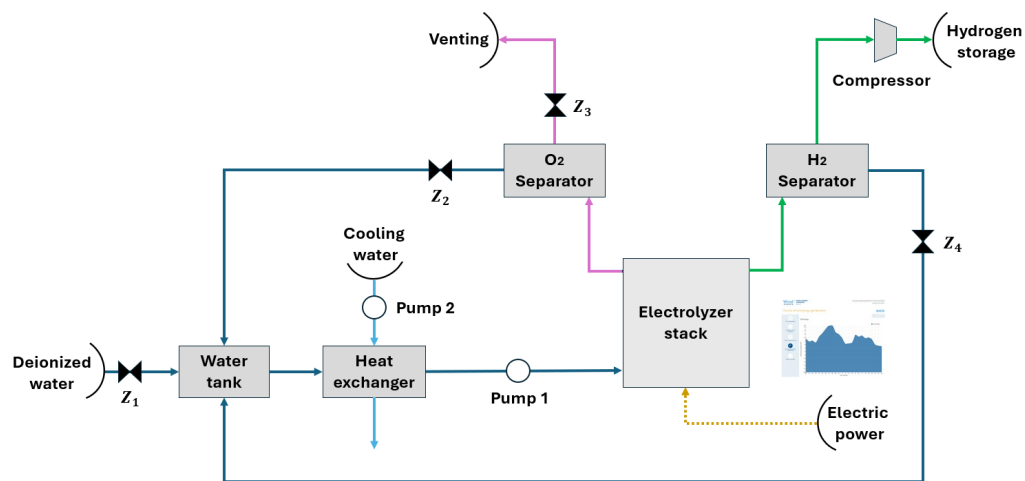
Fluctuations and Safety



- Major safety risk:
 - H_2/O_2 mixtures are flammable
 - Safety limit:
2 vol%
 - Lower explosion limit:
4 vol%



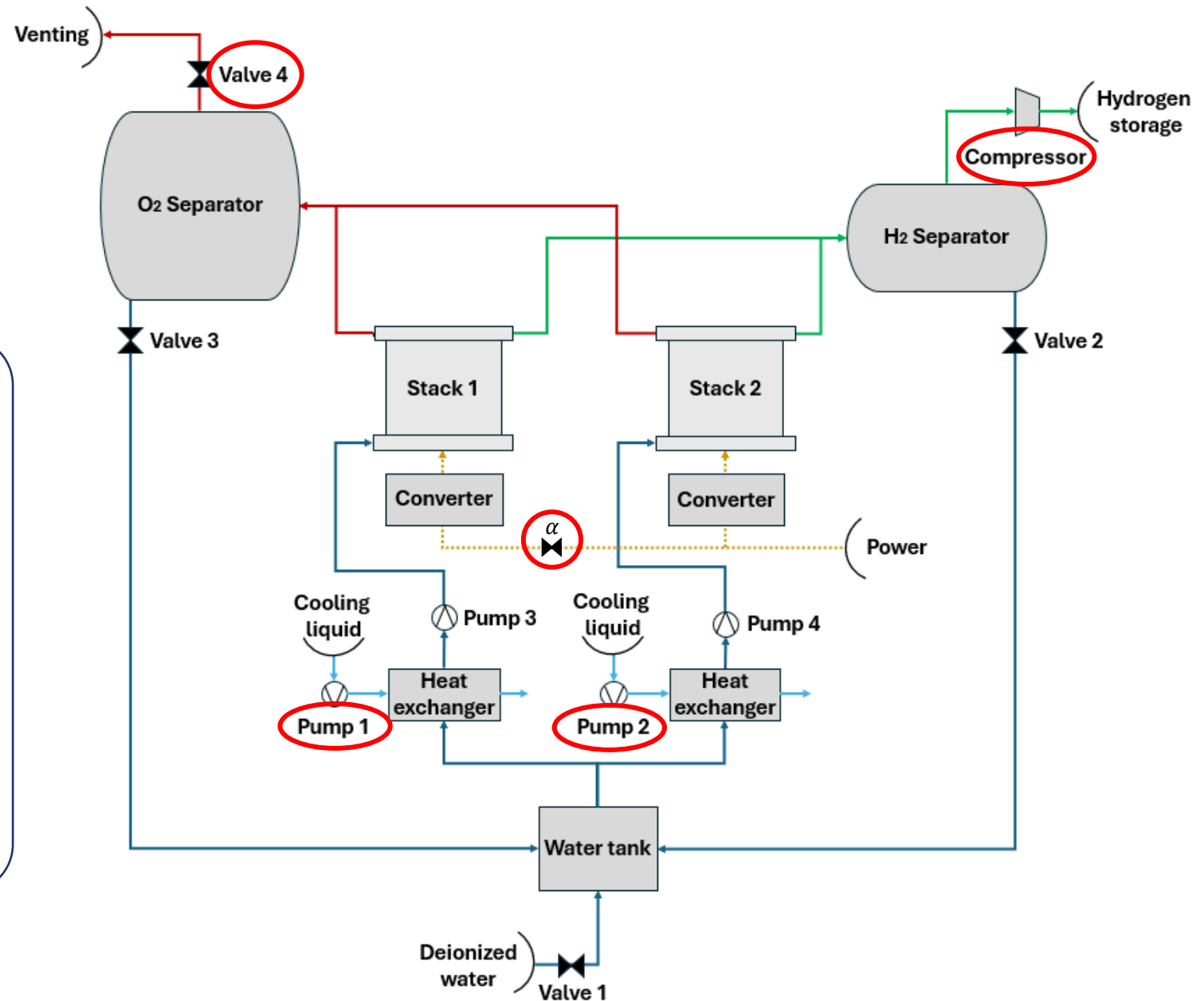
Two-Stack System Description



Available Actuators

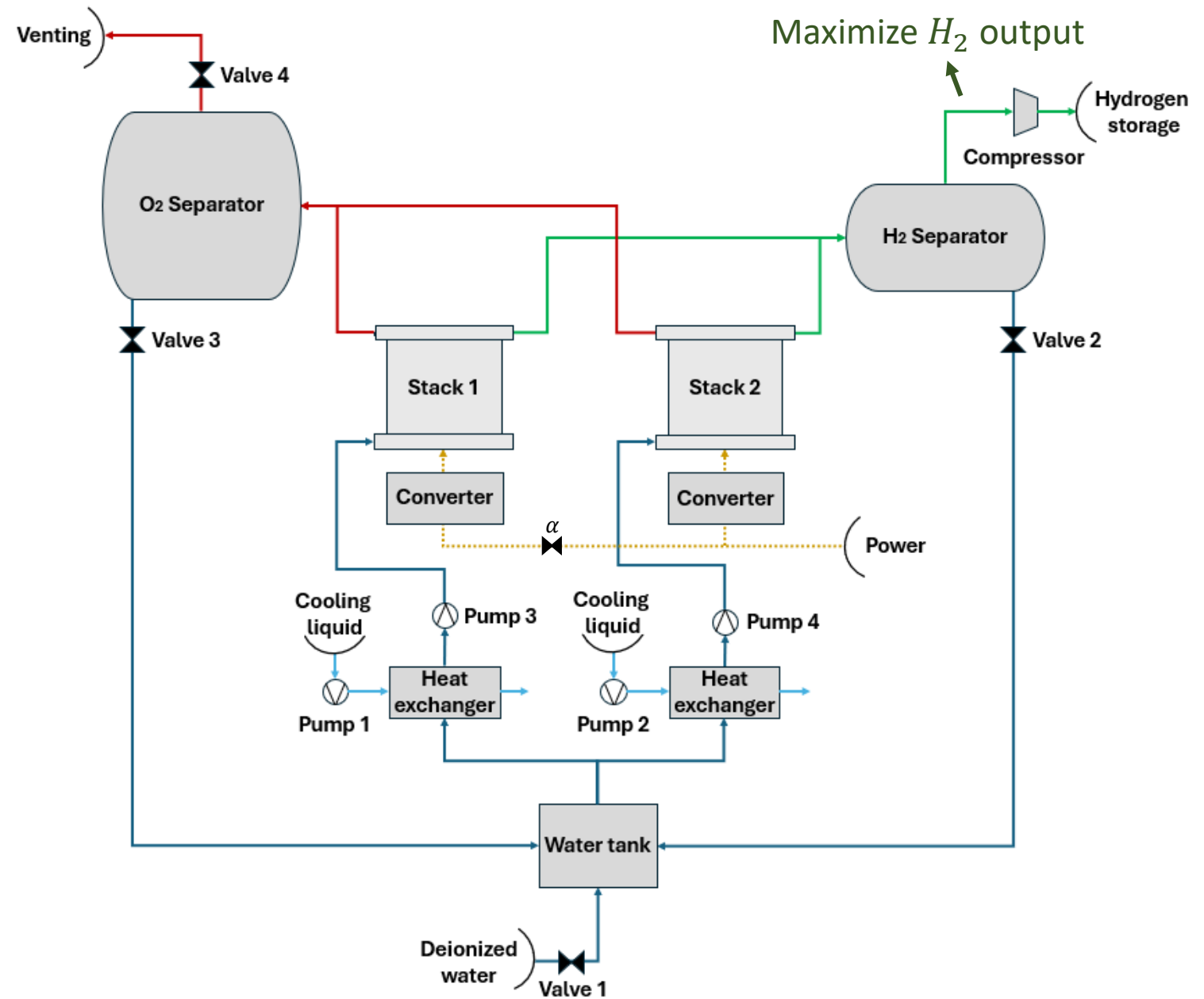
5 available actuators after level control:

- Oxygen purge
- Hydrogen flow rate
- Power allocation between the stacks
- Cooling liquid flow rates



Optimization

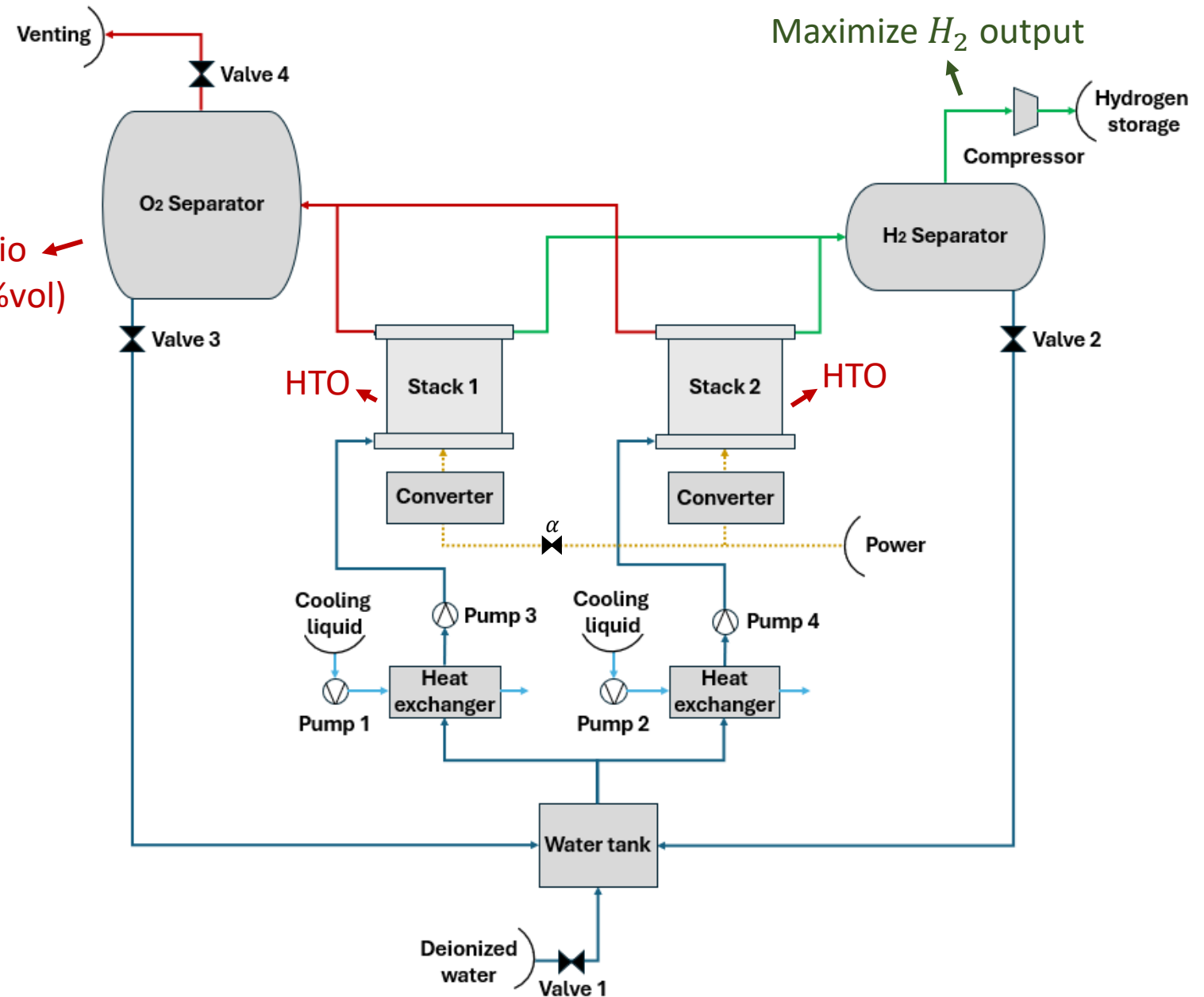
- Objective



Optimization

- Objective
- Constraints

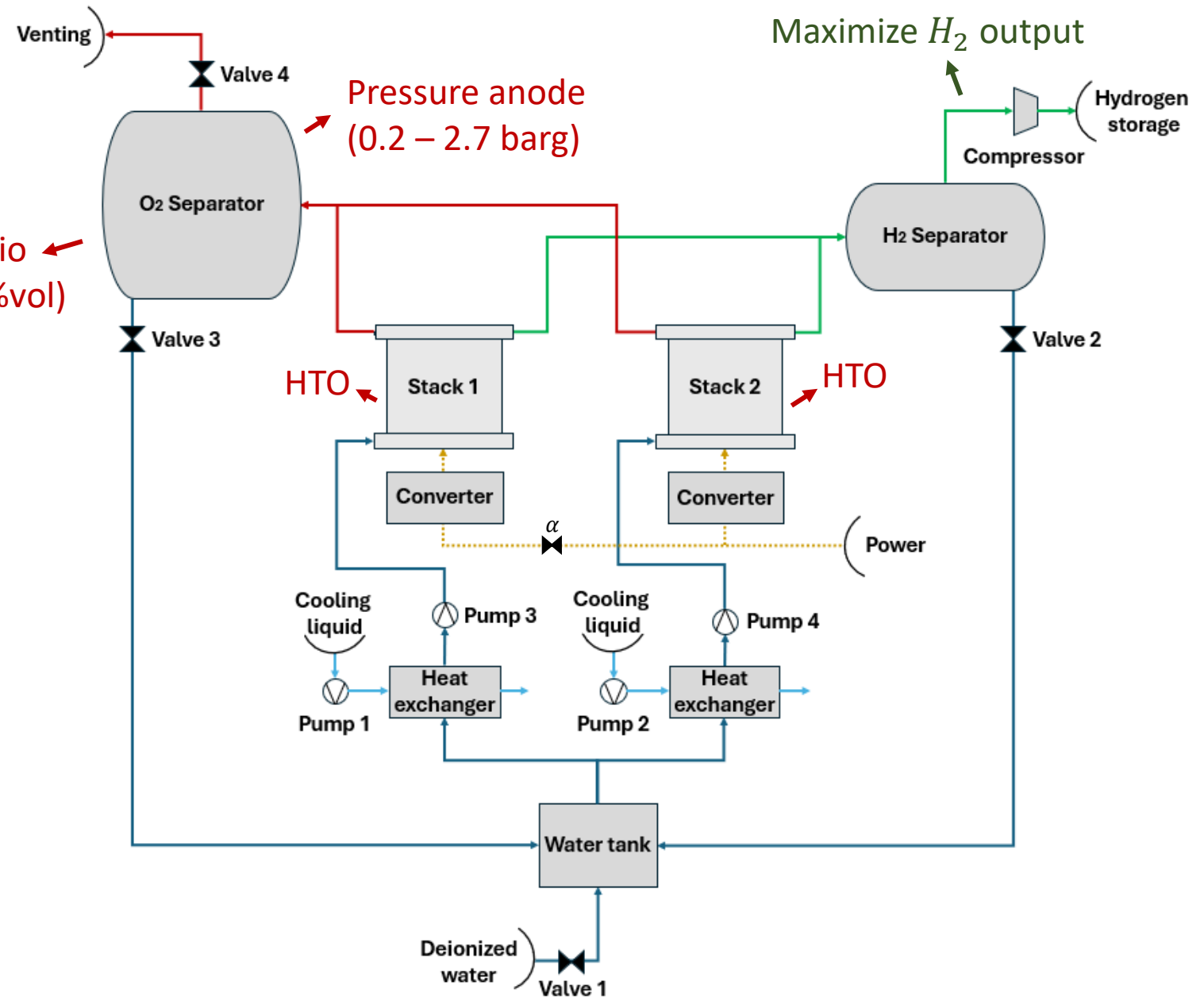
H_2 to O_2 ratio
HTO (0 – 2 %vol)



Optimization

- Objective
- Constraints

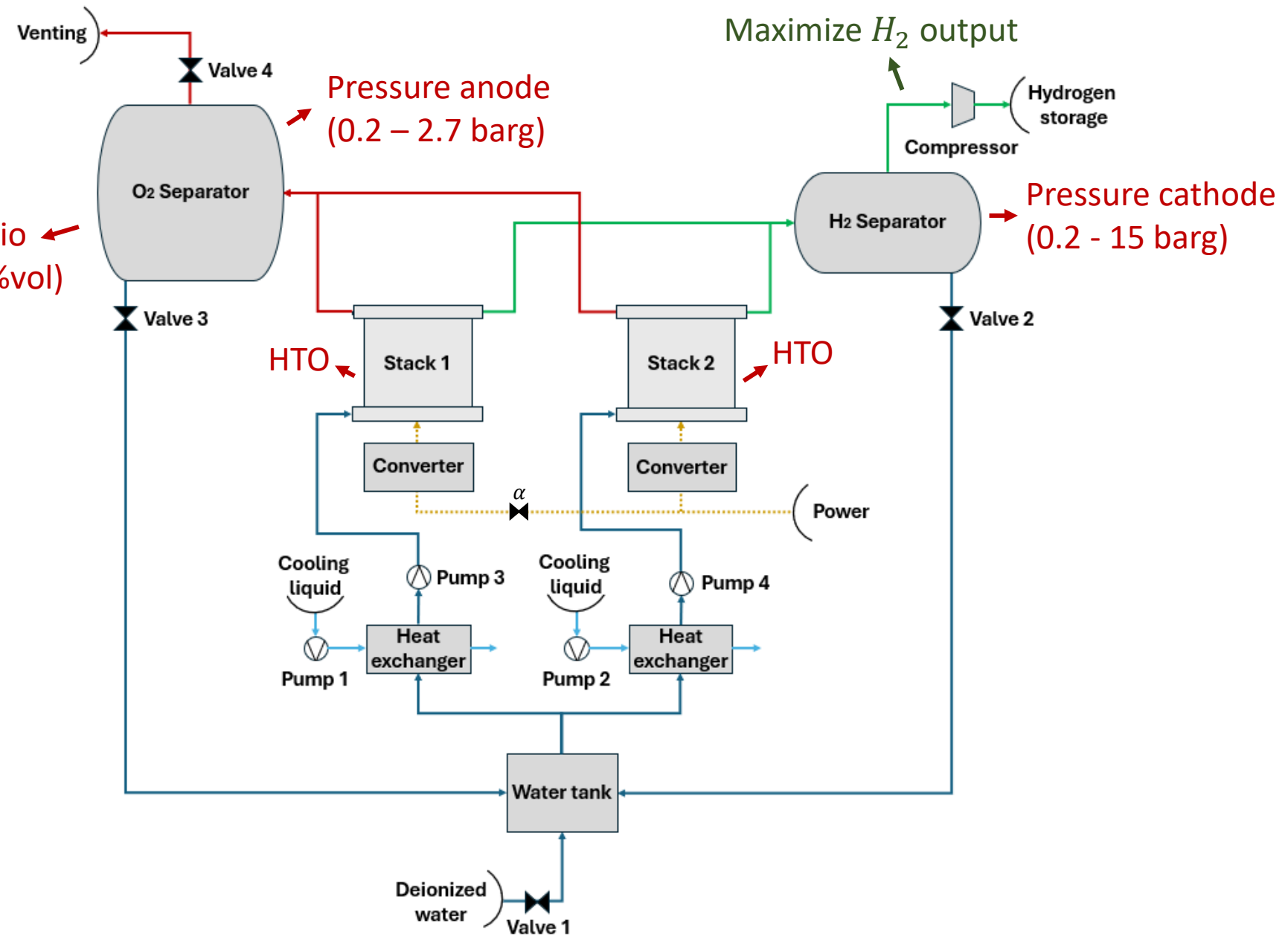
H_2 to O_2 ratio
HTO (0 – 2 %vol)



Optimization

- Objective
- Constraints

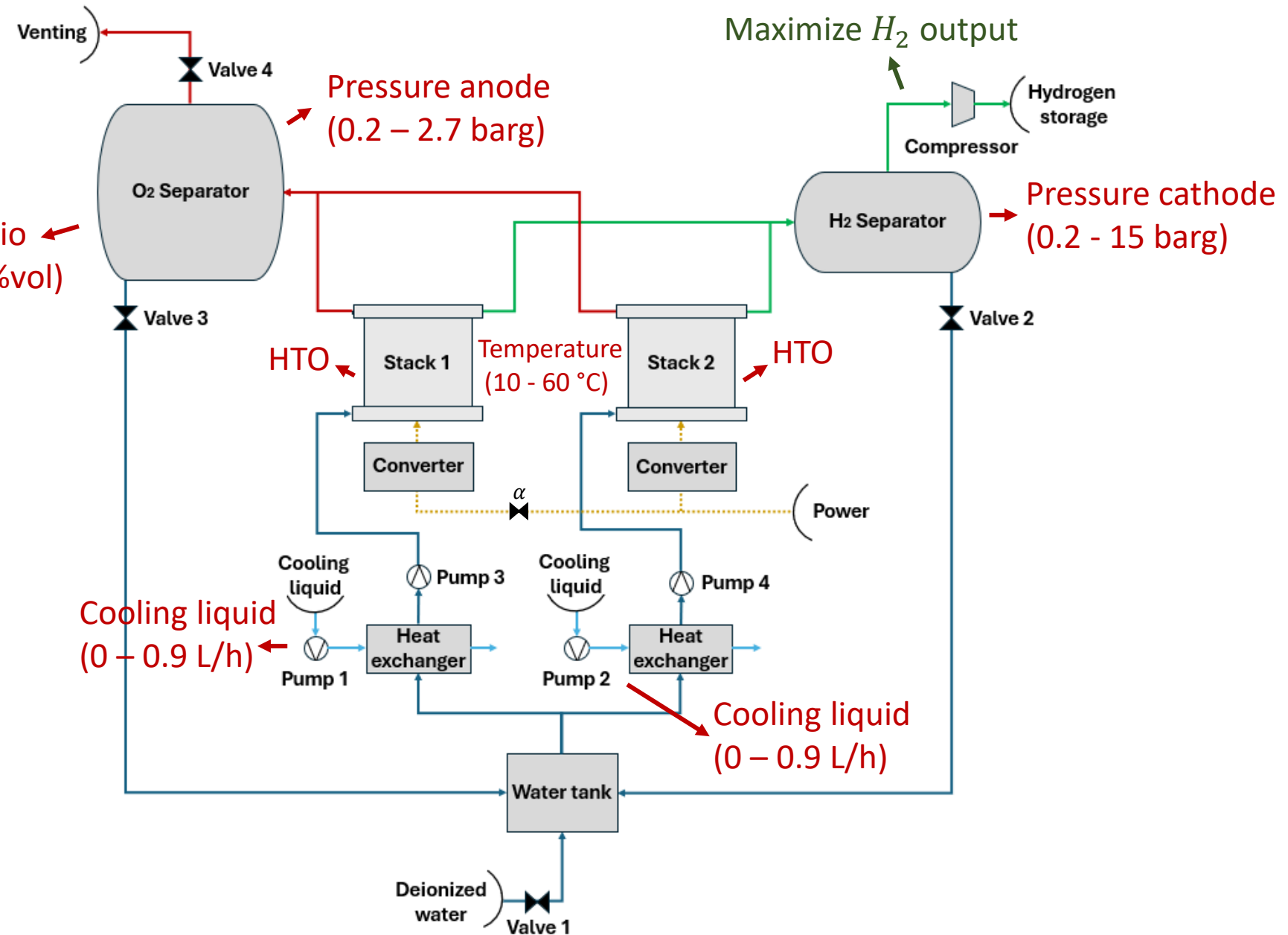
H_2 to O_2 ratio
HTO (0 – 2 %vol)



Optimization

- Objective
- Constraints

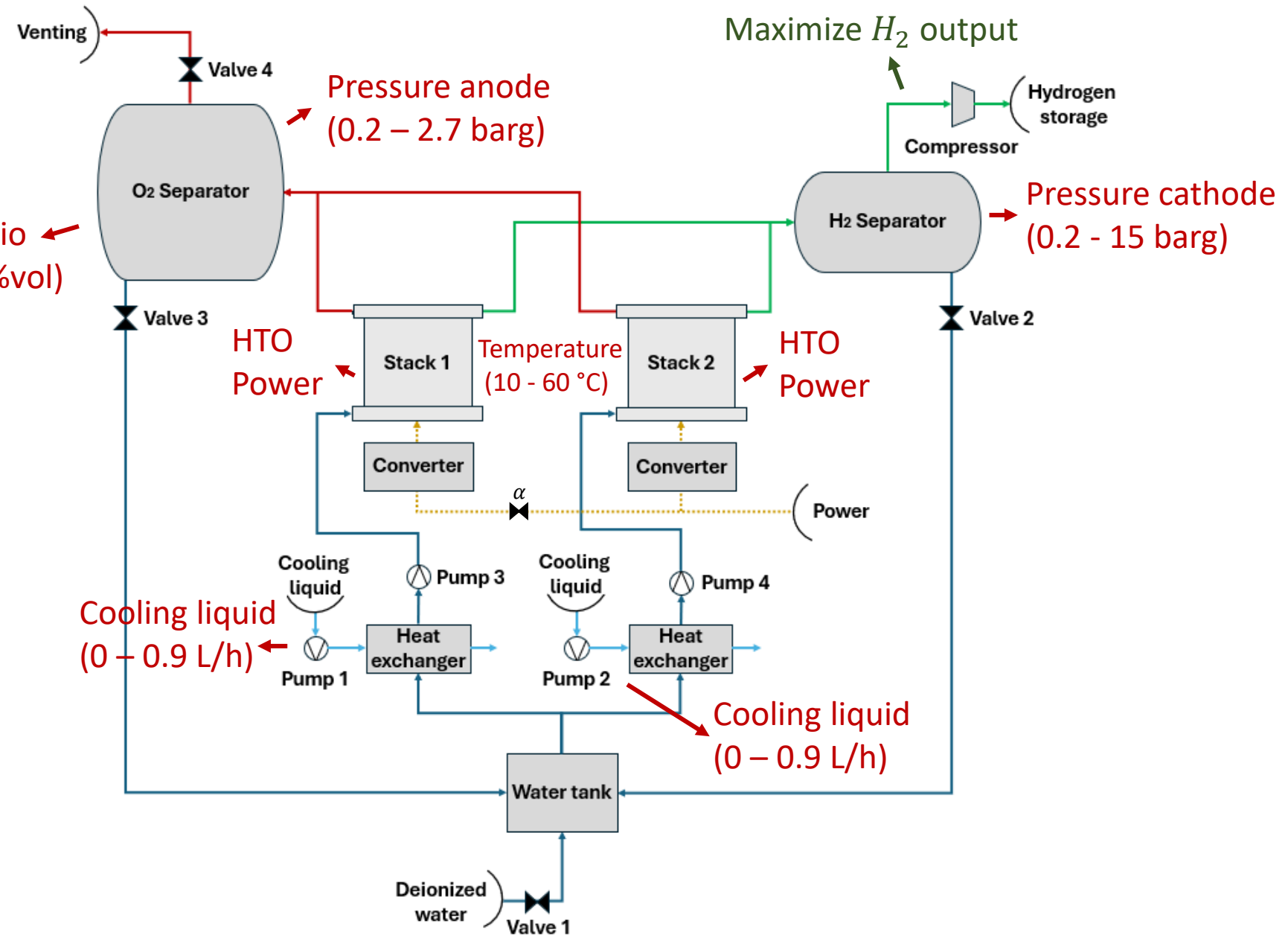
H_2 to O_2 ratio
HTO (0 – 2 %vol)



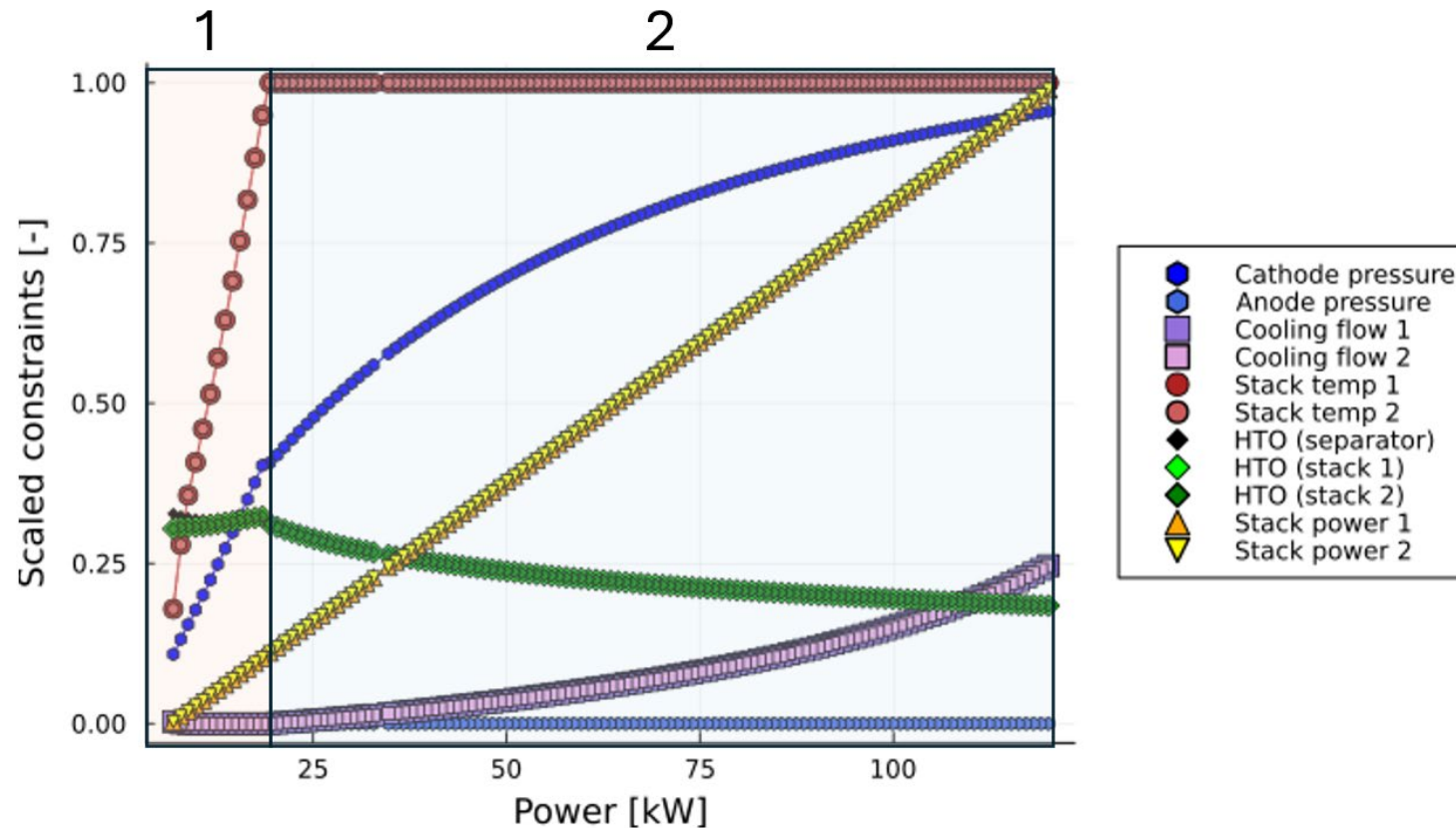
Optimization

- Objective
- Constraints

H_2 to O_2 ratio
HTO (0 – 2 %vol)



Optimal Operating Regime – Identical Stacks



Main takeaways

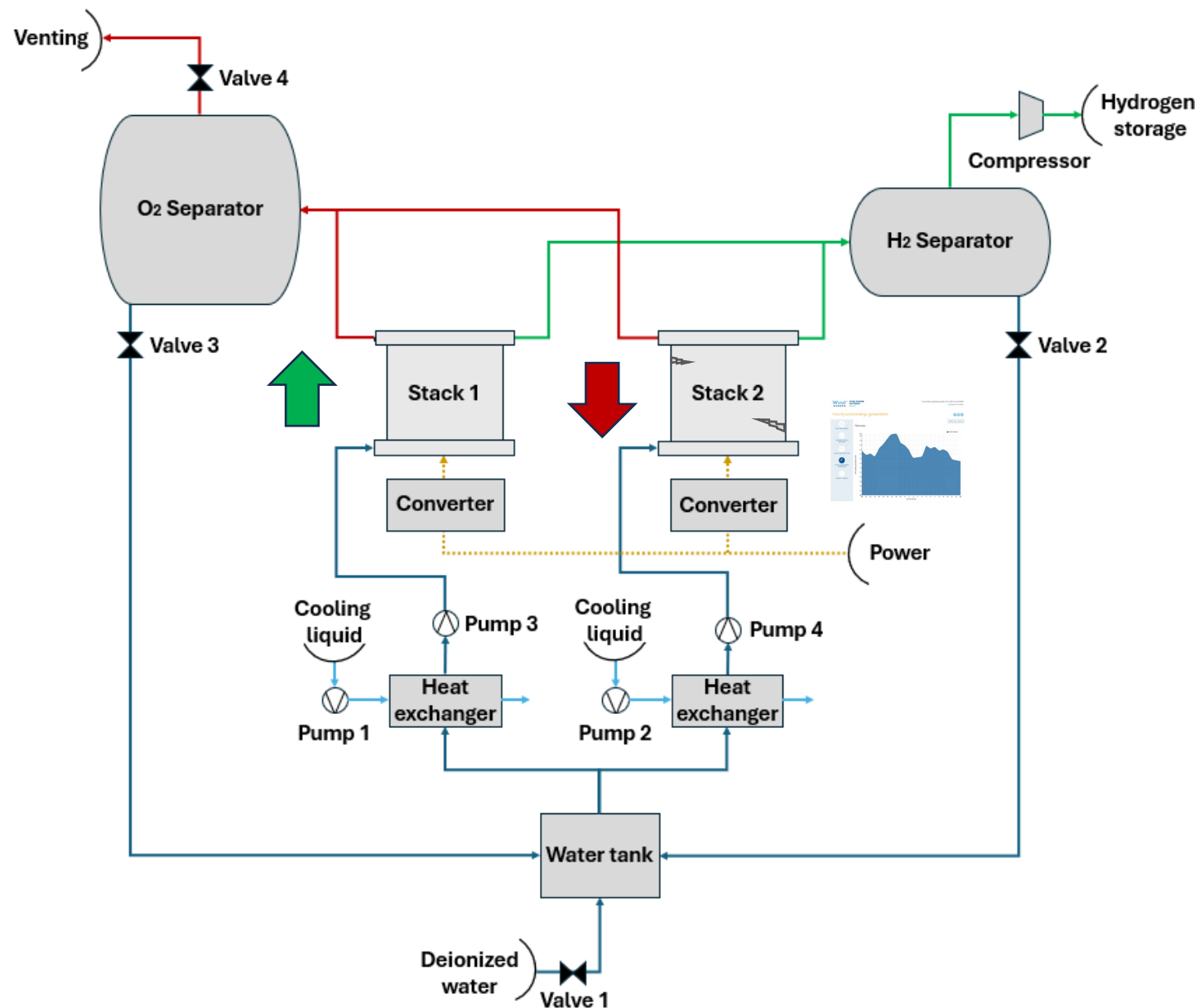
- 2 active constraint regions
- Divides power equally between stacks
- Closely resembles a single-stack system

Two-Stack System Description

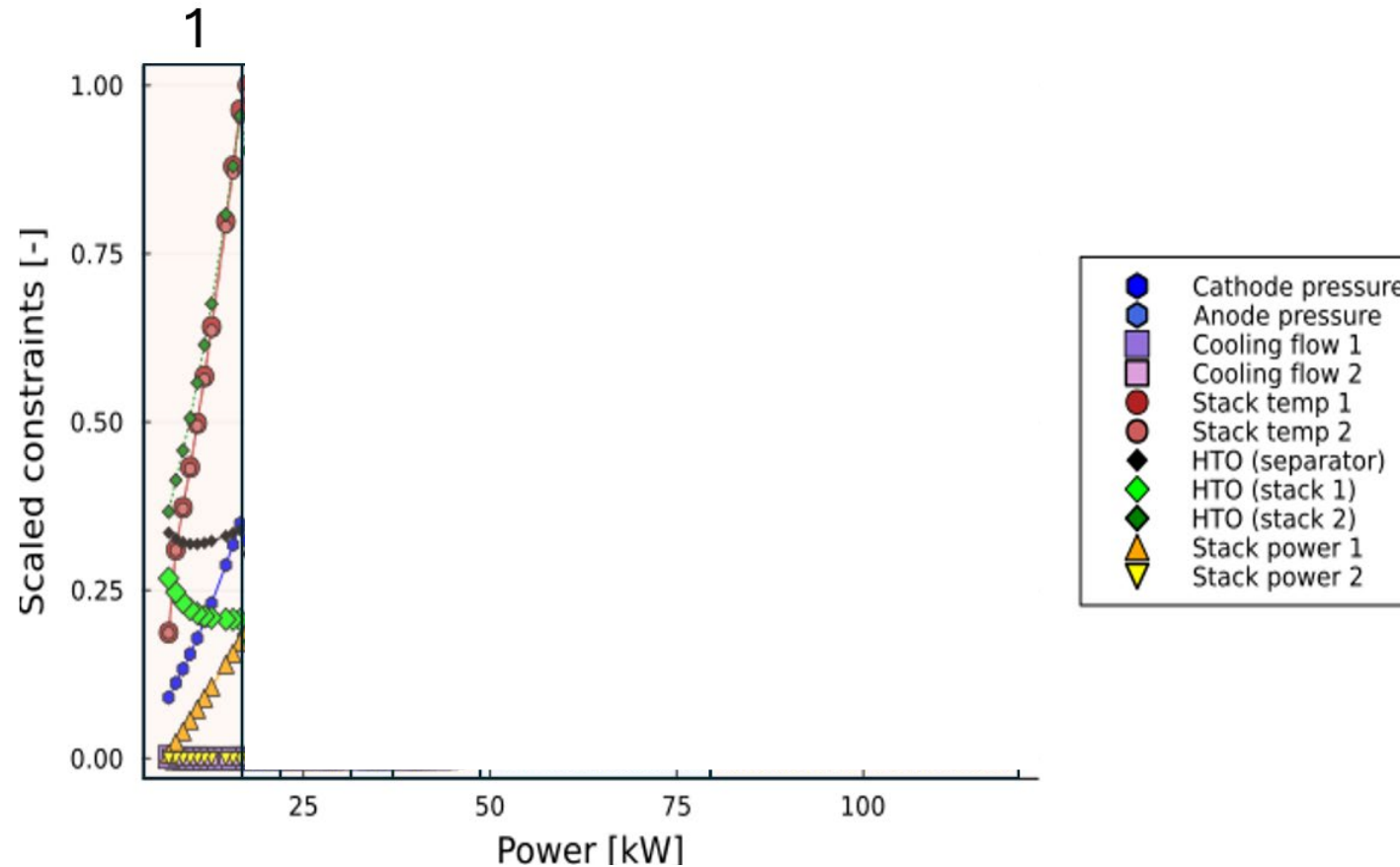
Non-identical stacks

- Stack 1 – 100%
- Stack 2 – 75%

Degradation and stack difference are represented through reduced Faraday efficiency



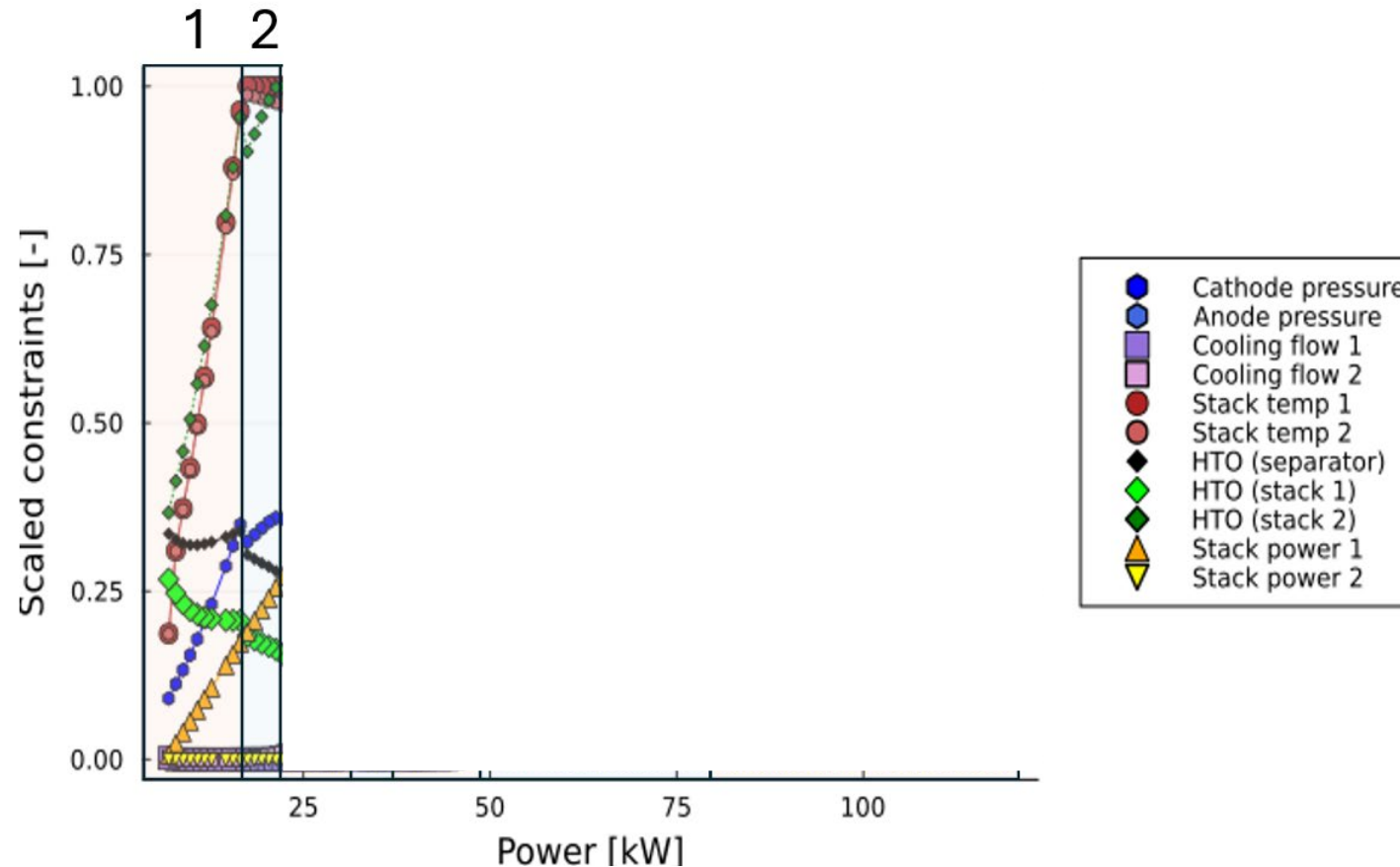
Optimal Operating Regime – Non-Identical Stacks (75%)



Observations

- 7 active constraint regions
- Preferentially loads Stack 1 (most efficient stack)
- HTO constraint active for Stack 2 (least efficient stack)
- Uses both power and pressure gradient to maintain HTO

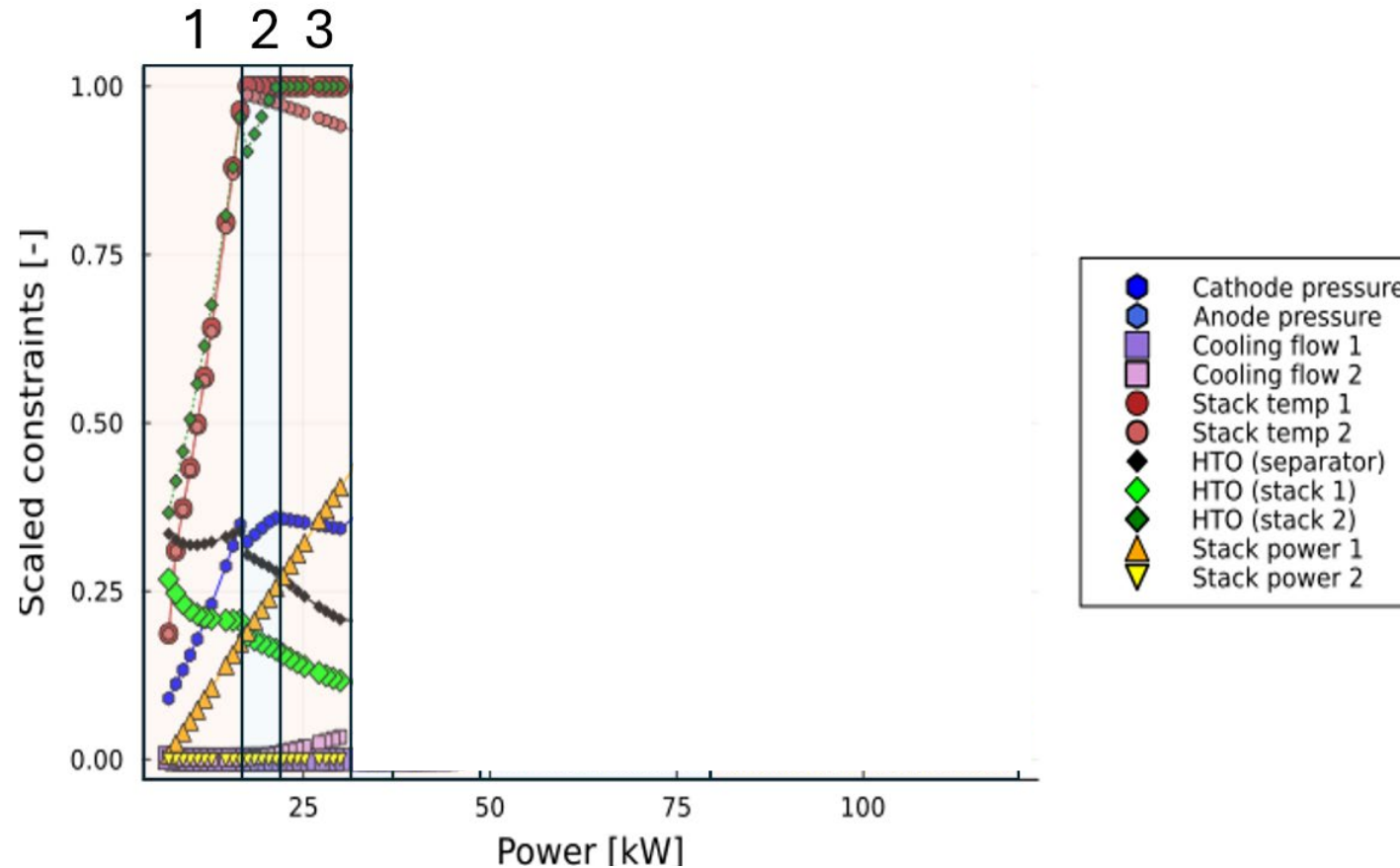
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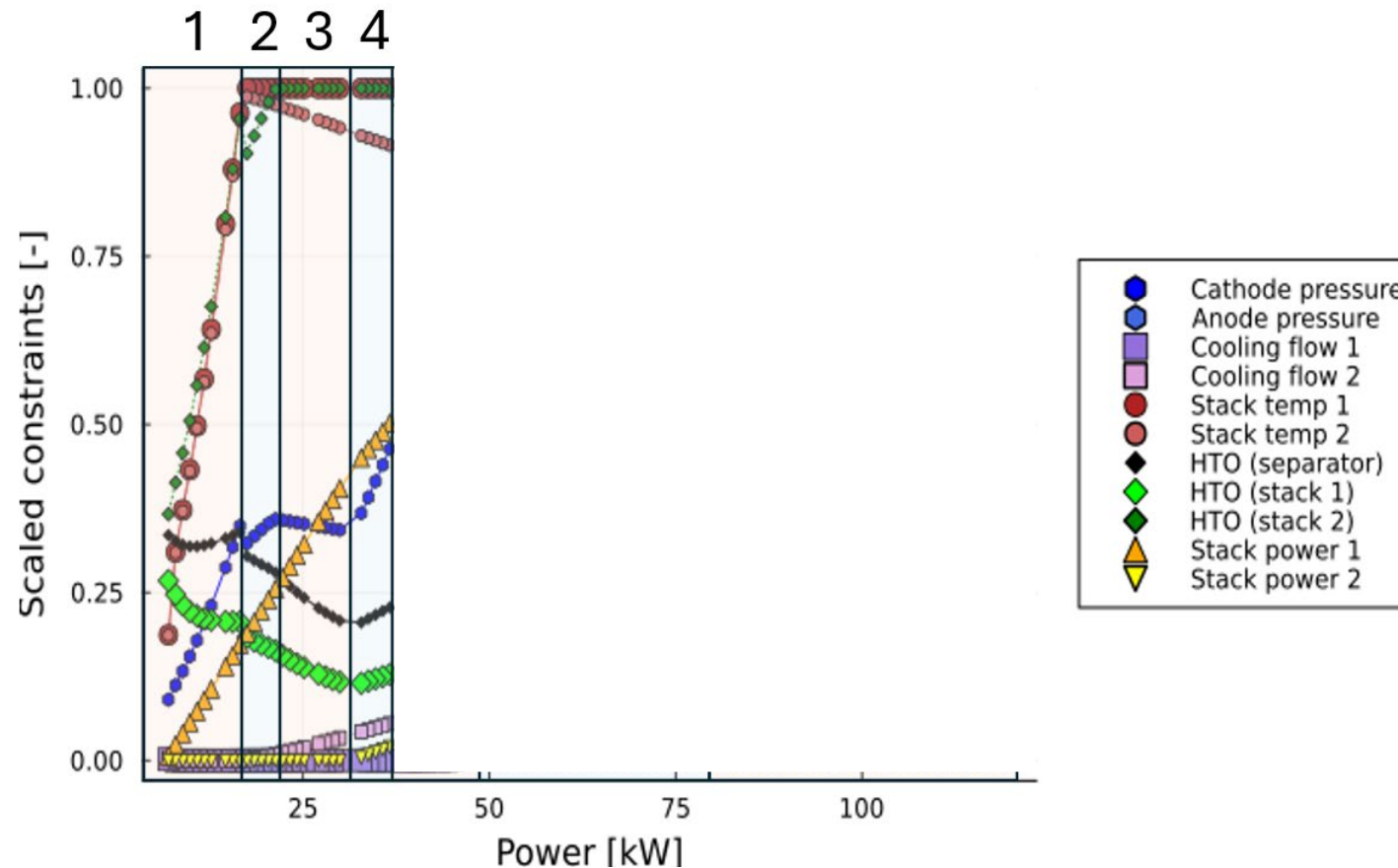
Optimal Operating Regime – Non-Identical Stacks (75%)



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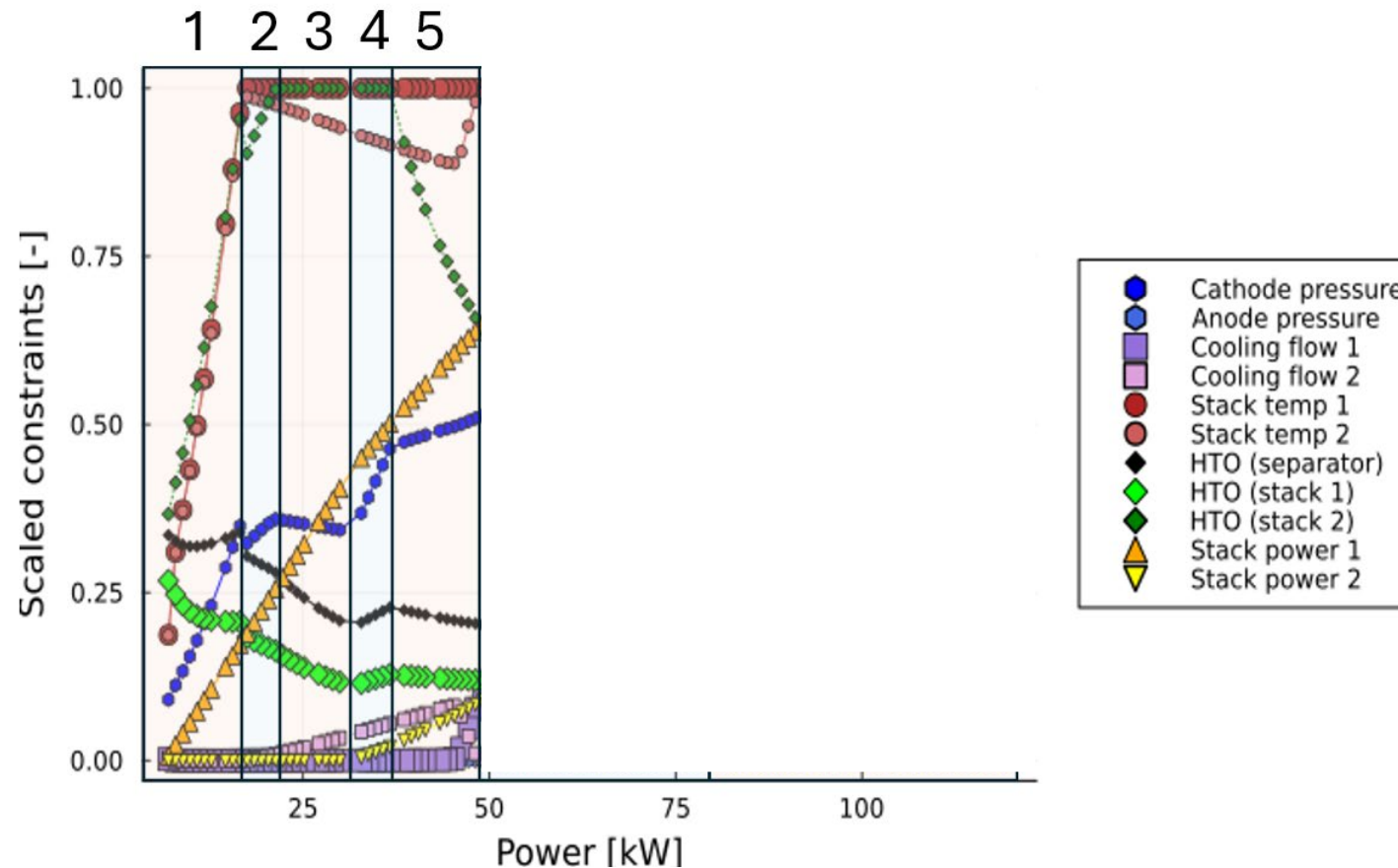
Optimal Operating Regime – Non-Identical Stacks (75%)



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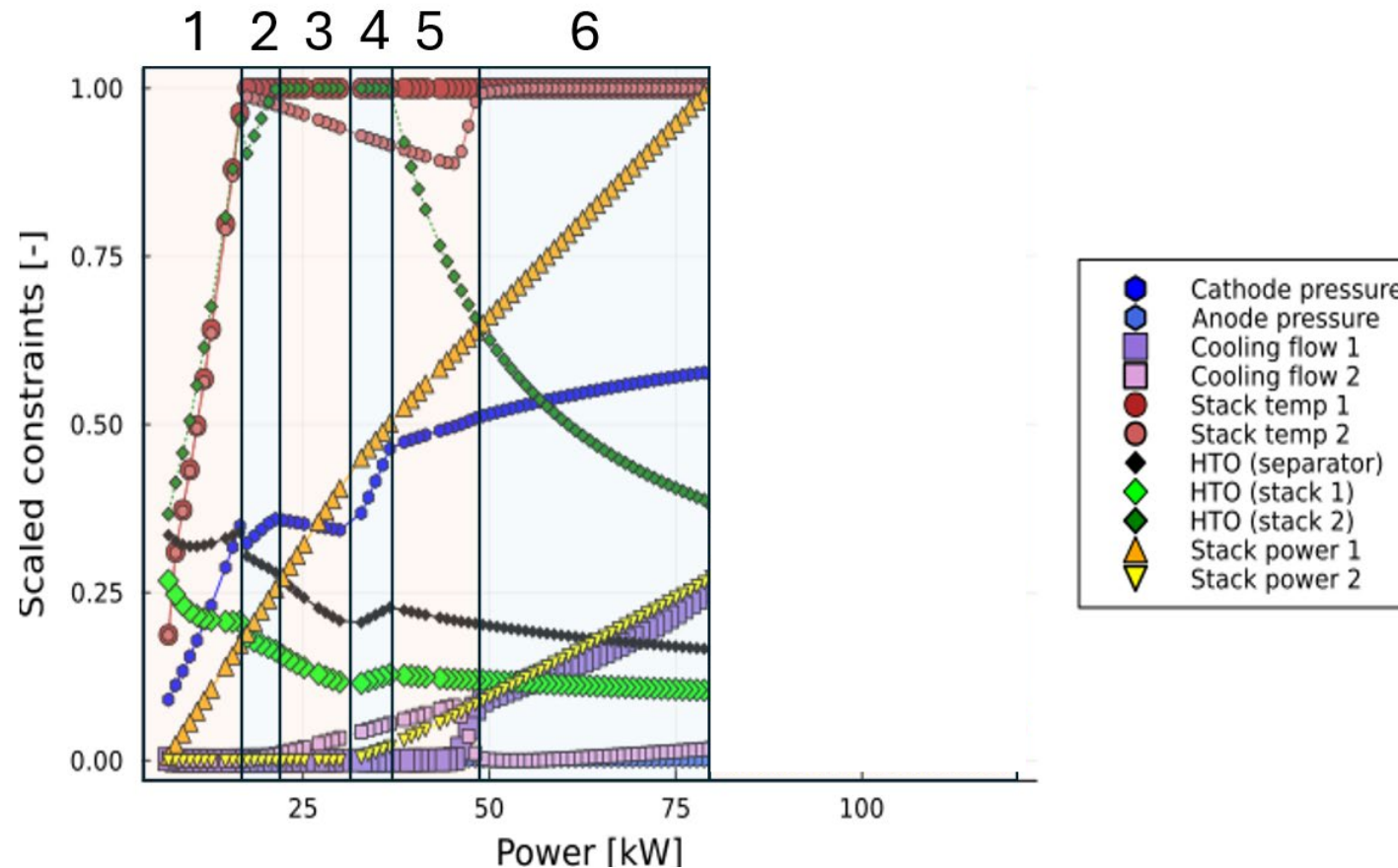
Optimal Operating Regime – Non-Identical Stacks (75%)



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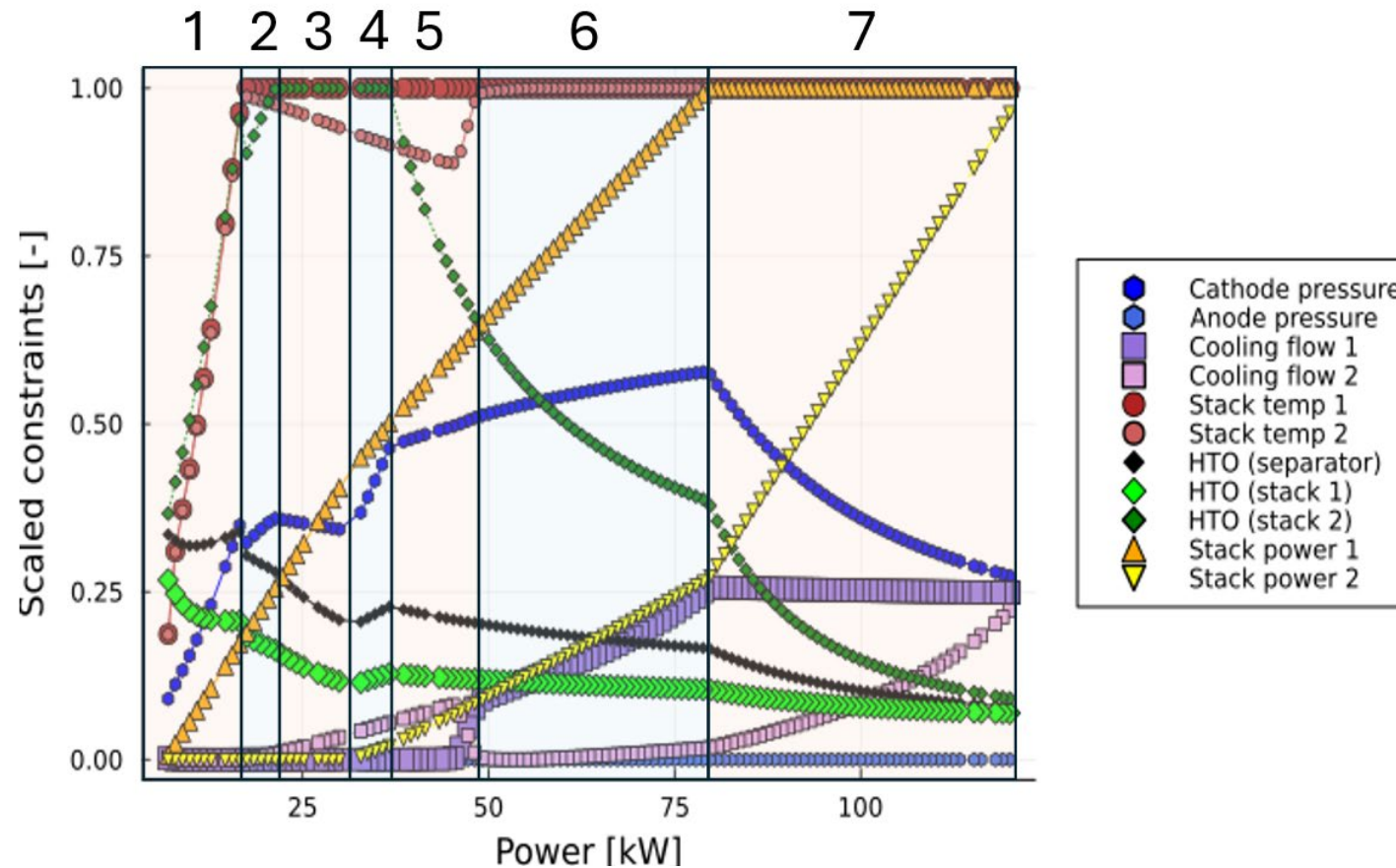
Optimal Operating Regime – Non-Identical Stacks (75%)



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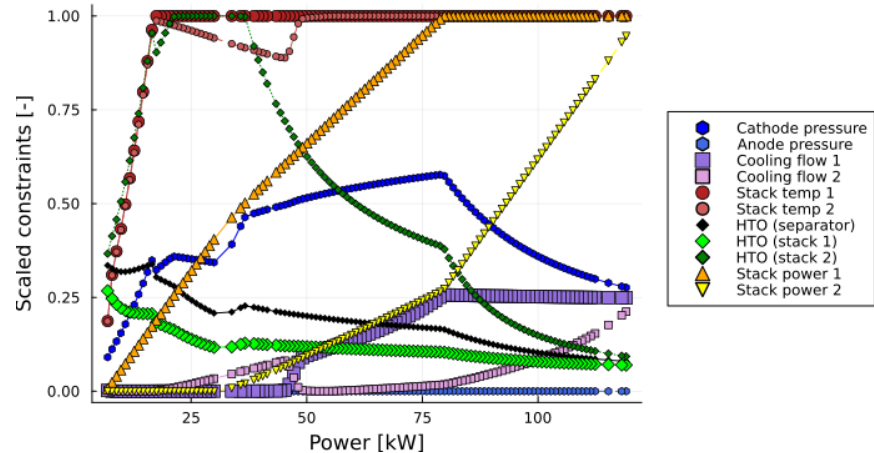
Optimal Operating Regime – Non-Identical Stacks (75%)



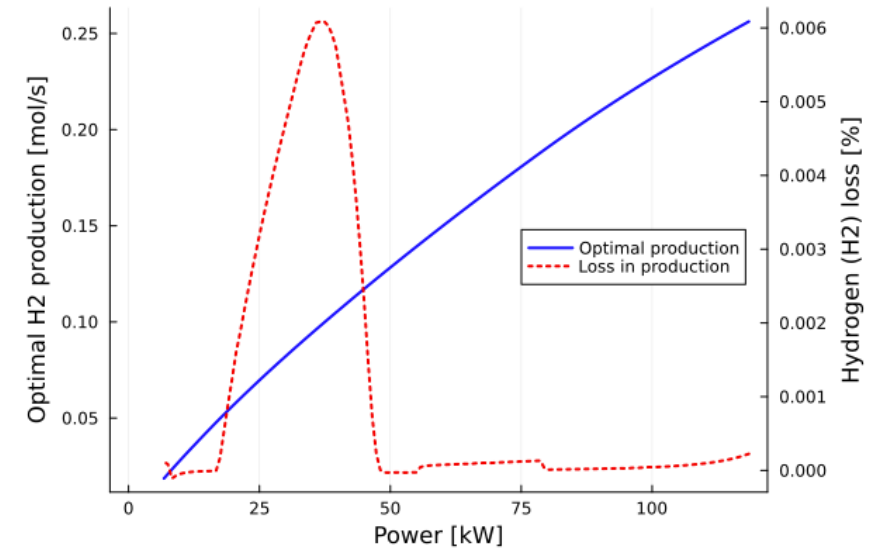
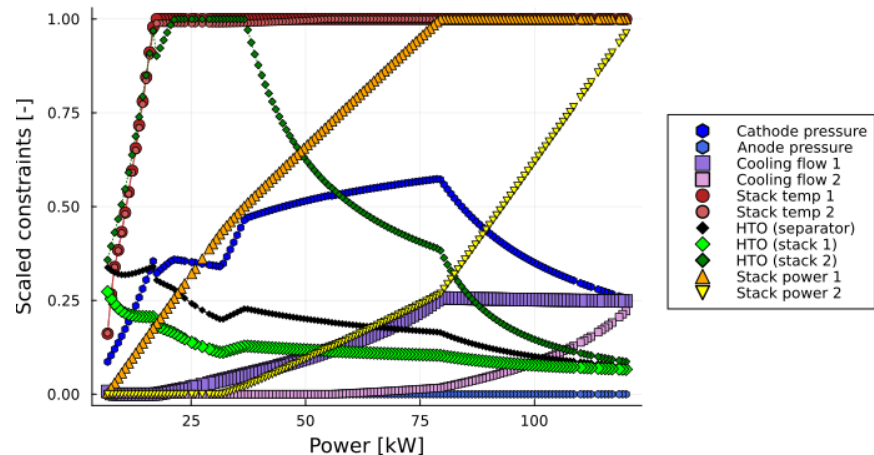
Observations

- 7 active constraint regions
- Preferentially loads Stack 1 (most efficient stack)
- HTO constraint active for Stack 2 (least efficient stack)
- Uses both power and pressure gradient to maintain HTO

Simplification – Increase Stack 2 Temperature



Objective: $\max H_2 - F_{cool,2}$



Observations

- Maximizing Stack 2 temperature gives a negligible loss in hydrogen production
- Stack 2 temperature becomes an active constraint, simplifying our system

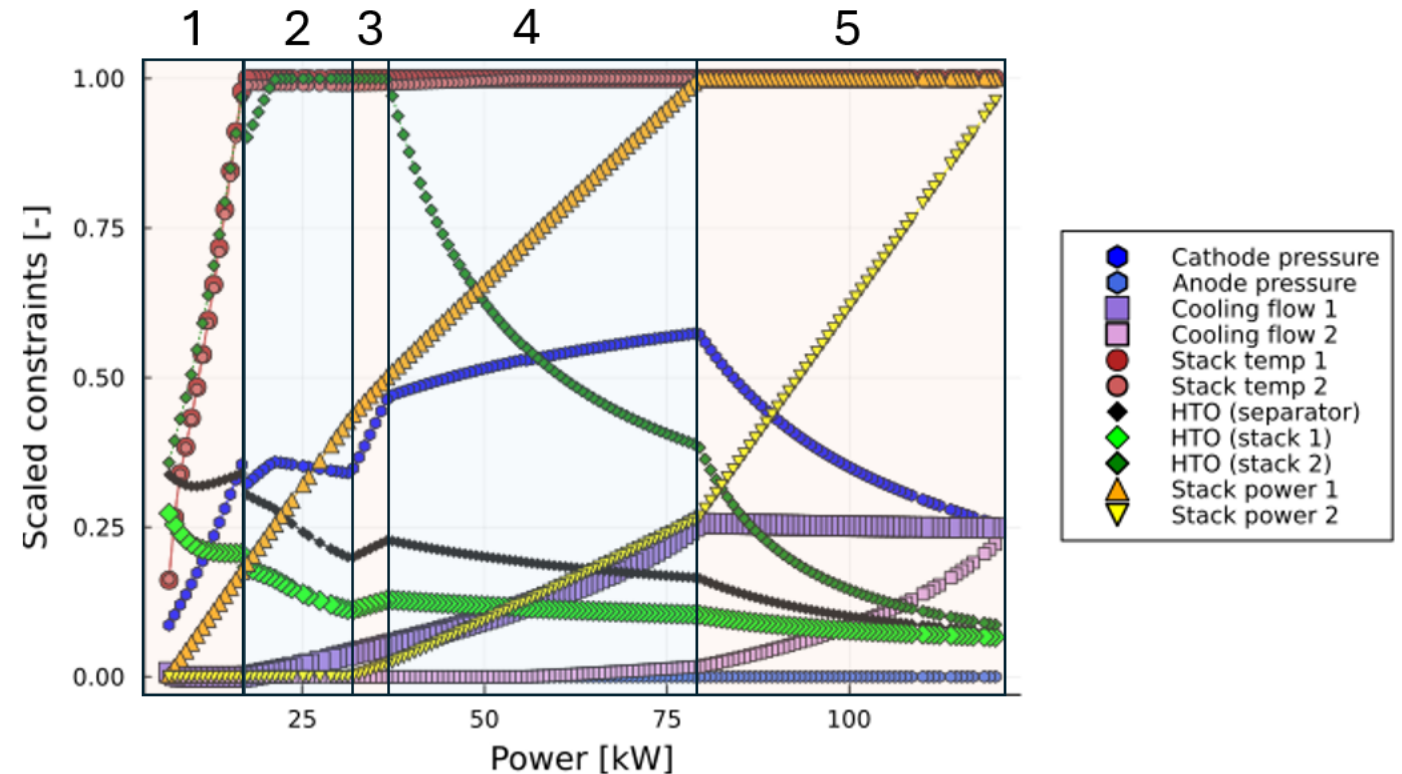
Control Design

5 Available actuators

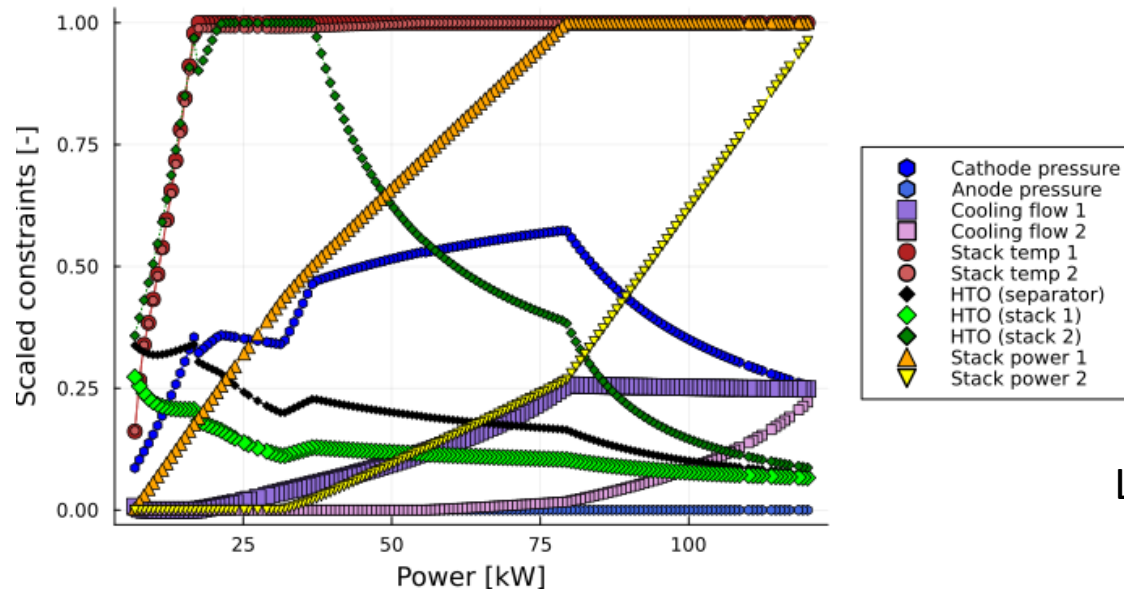
≥ 3 Active constraints (all regions)

- Anode pressure
- Stack 1 temperature/cooling
- Stack 2 temperature/cooling

=> 2 DoFs after active constraints

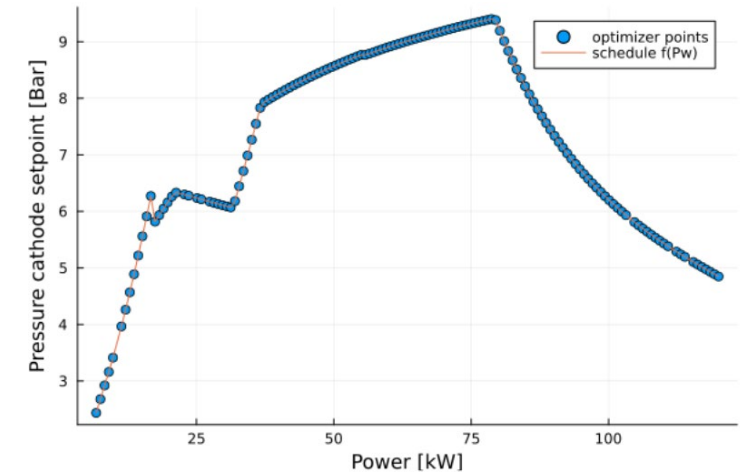


Optimal Reference Values – HTO Constrained

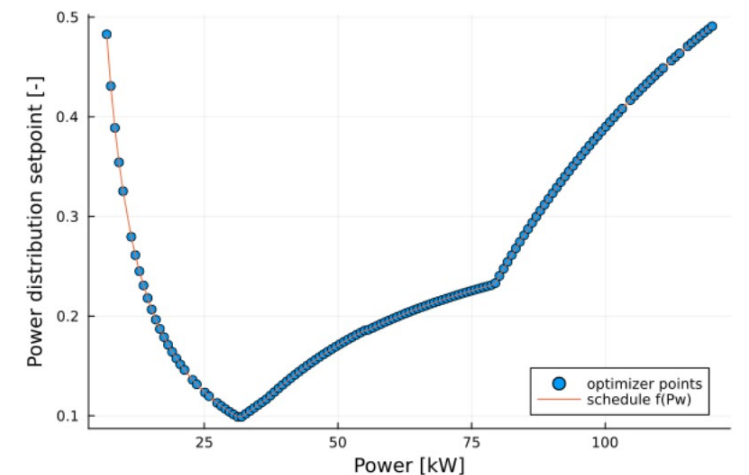


Linear interpolation

Optimal cathode pressure



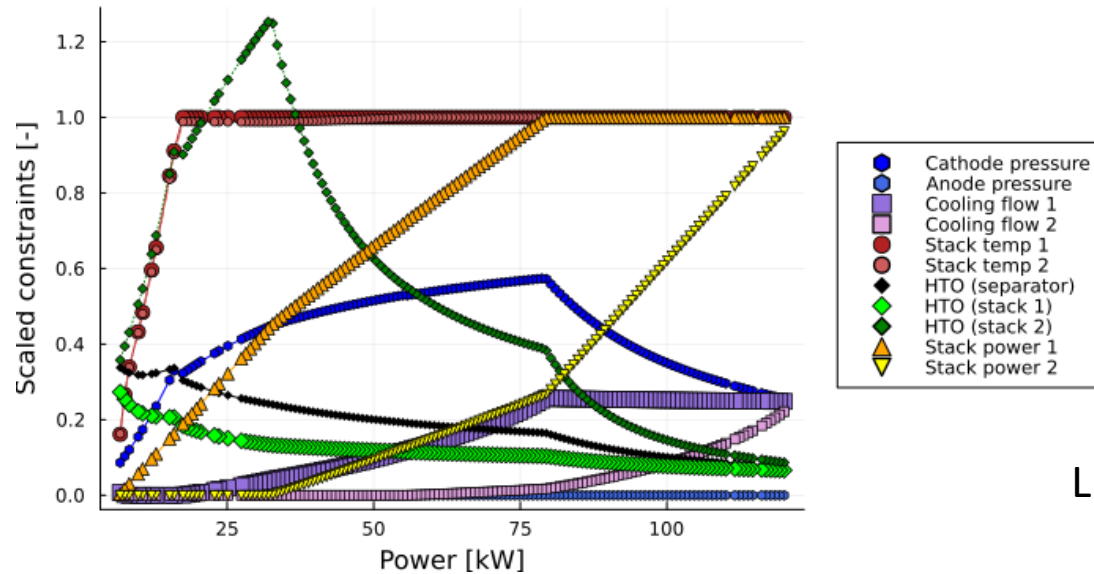
Optimal power distribution



Remarks

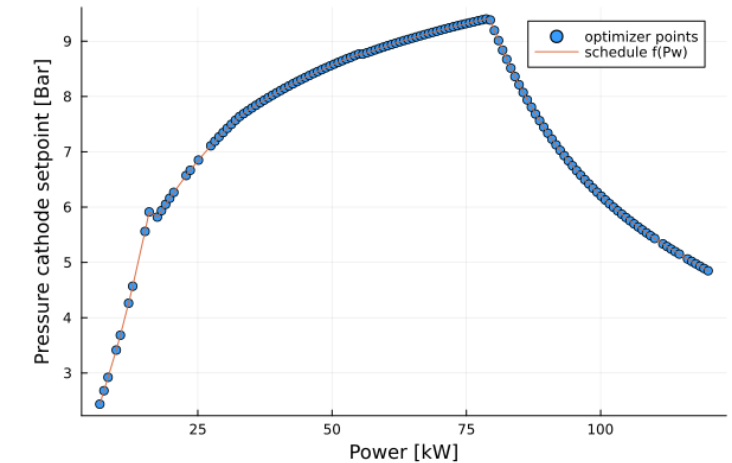
- The pressure and power distribution determine the HTO
- What if we have a model mismatch?

Optimal Reference Values – No HTO Constraint

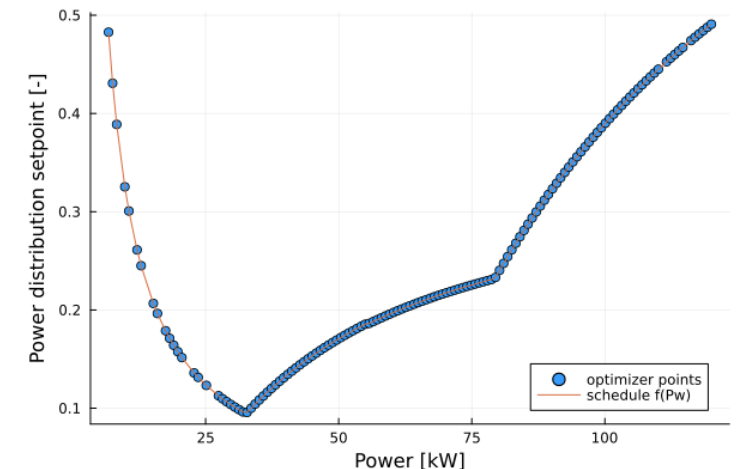


Linear interpolation

Optimal cathode pressure



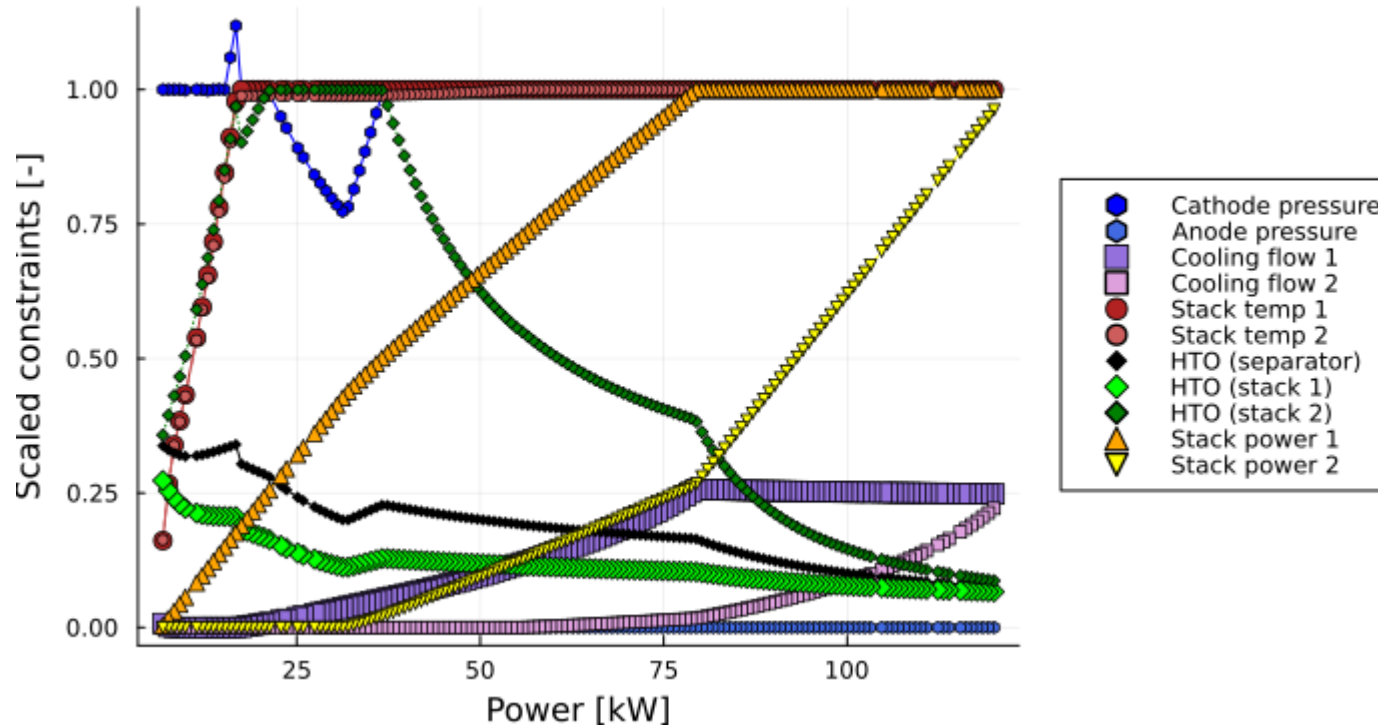
Optimal power distribution



Observations

- The optimal operating regime is very similar; however, we may use higher cathode pressures at lower power

Cathode pressure-HTO Relationship



Remarks

- We use the cathode reference value as its scaled upper constraint

Observations

- We have a small section where the unconstrained optimum cathode pressure reference is smaller than the constrained one
- The cathode pressure and the HTO of Stack 2 swap between being active constraints (can be facilitated using selectors)

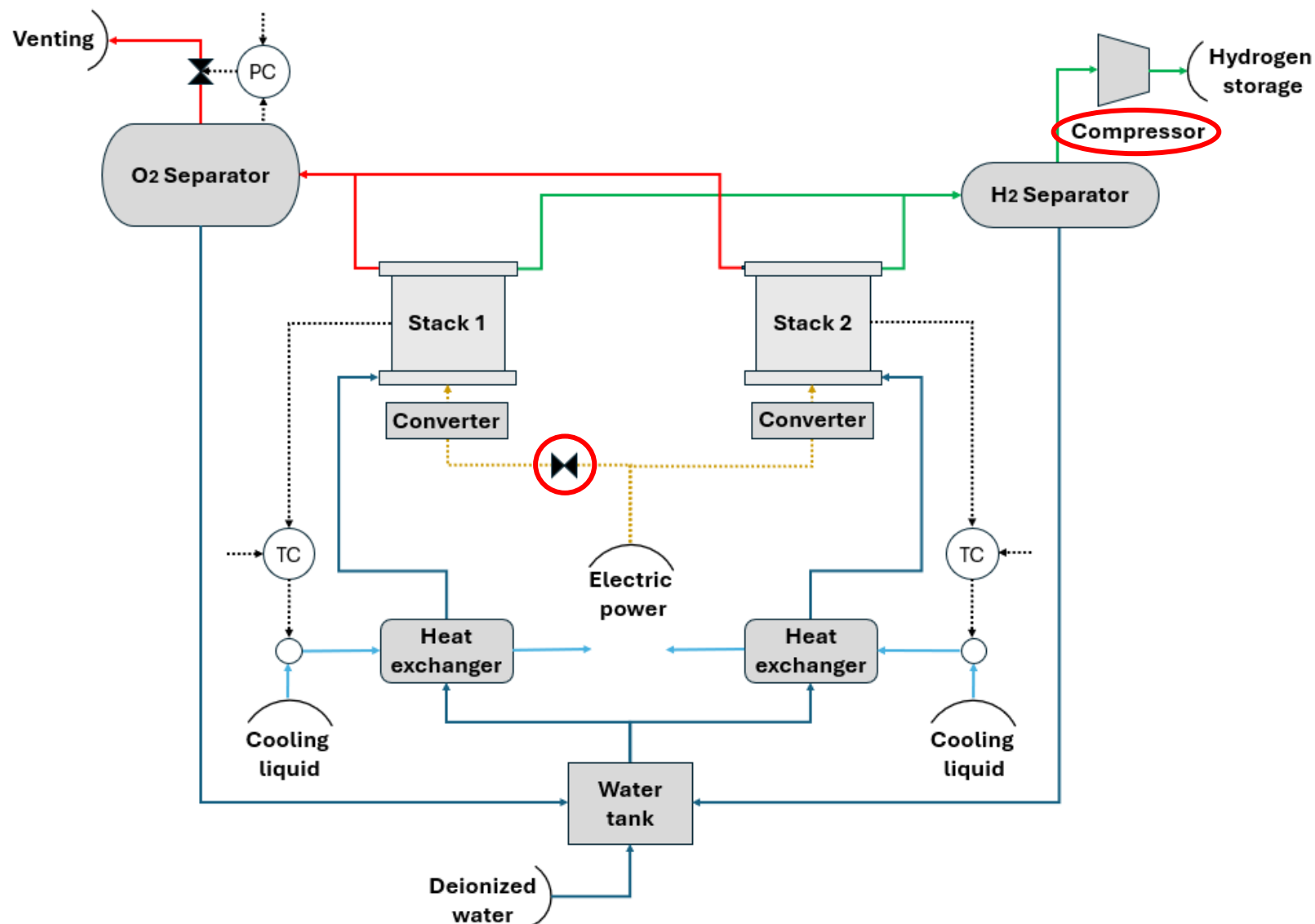
Control Active Constraints

Active Constraints

- Oxygen pressure
- Temperature Stack 1
- Temperature Stack 2

Remaining DoFs

- Power distributor
- Hydrogen compressor



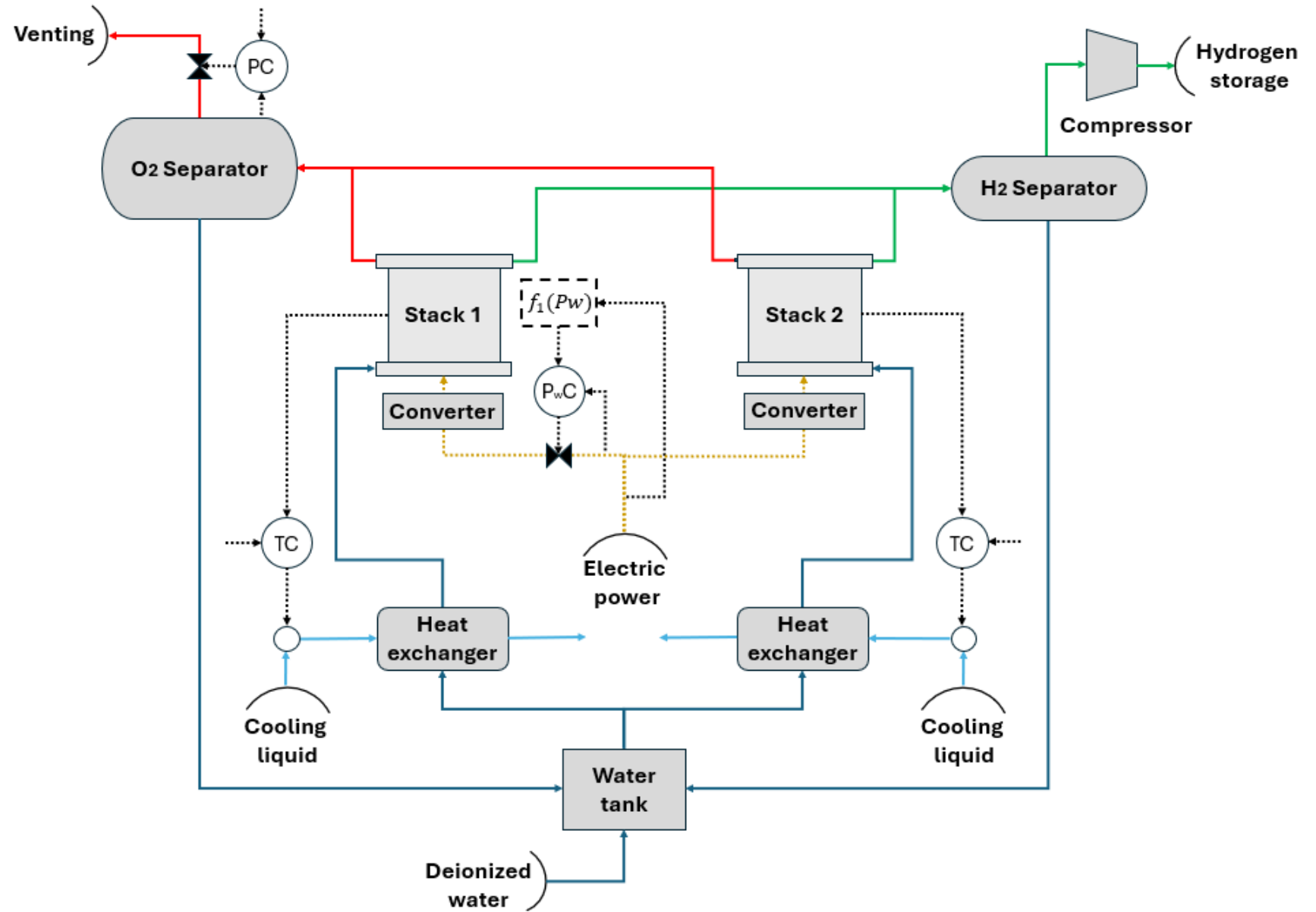
Setpoint Scheduling

Active Constraints

- Oxygen pressure
- Temperature Stack 1
- Temperature Stack 2

Setpoint Scheduling

- Power distributor (f_1)



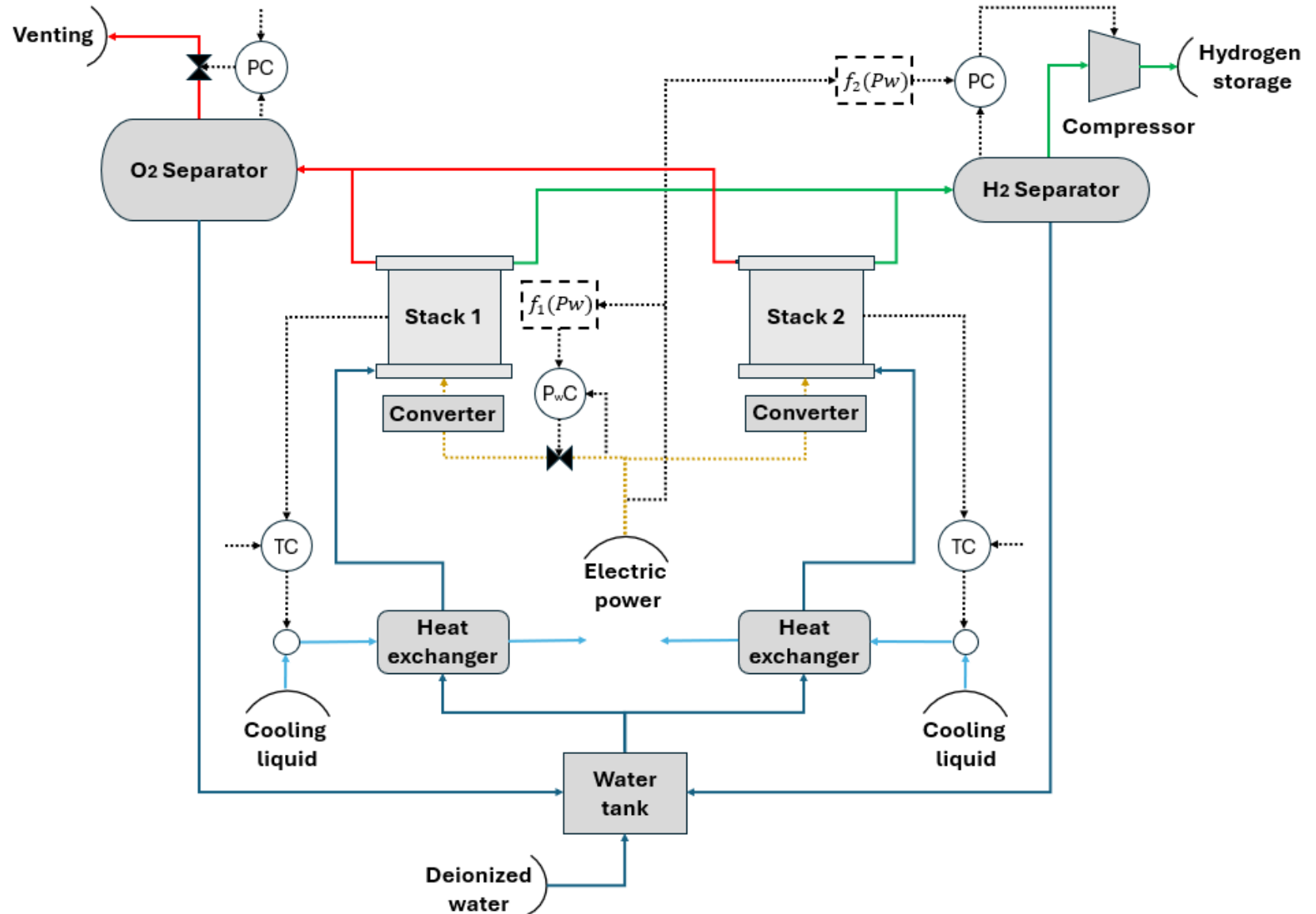
Setpoint Scheduling

Active Constraints

- Oxygen pressure
- Temperature Stack 1
- Temperature Stack 2

Setpoint Scheduling

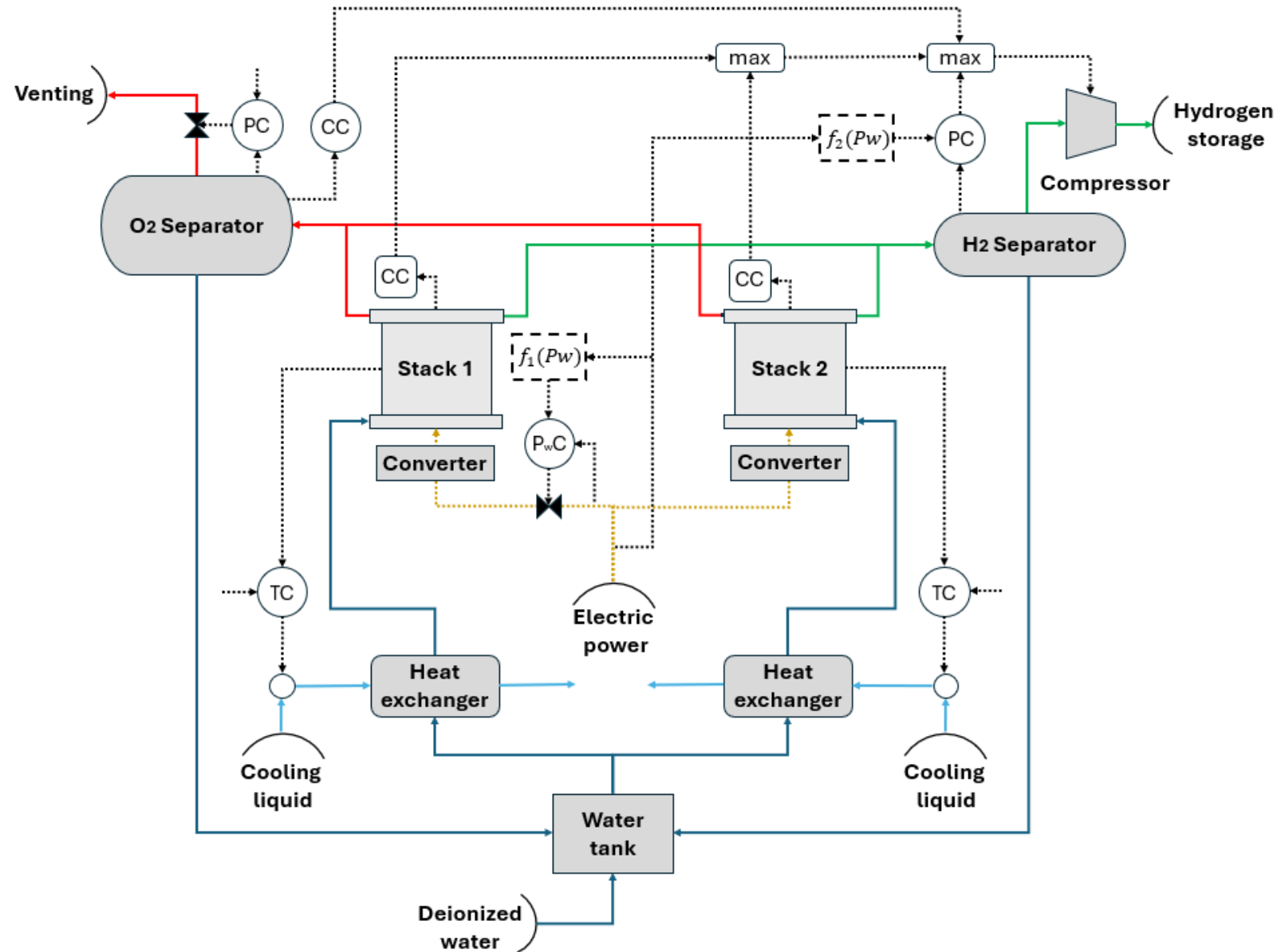
- Power distributor (f_1)
- Hydrogen pressure (f_2)



Selectors for Safety

Remarks

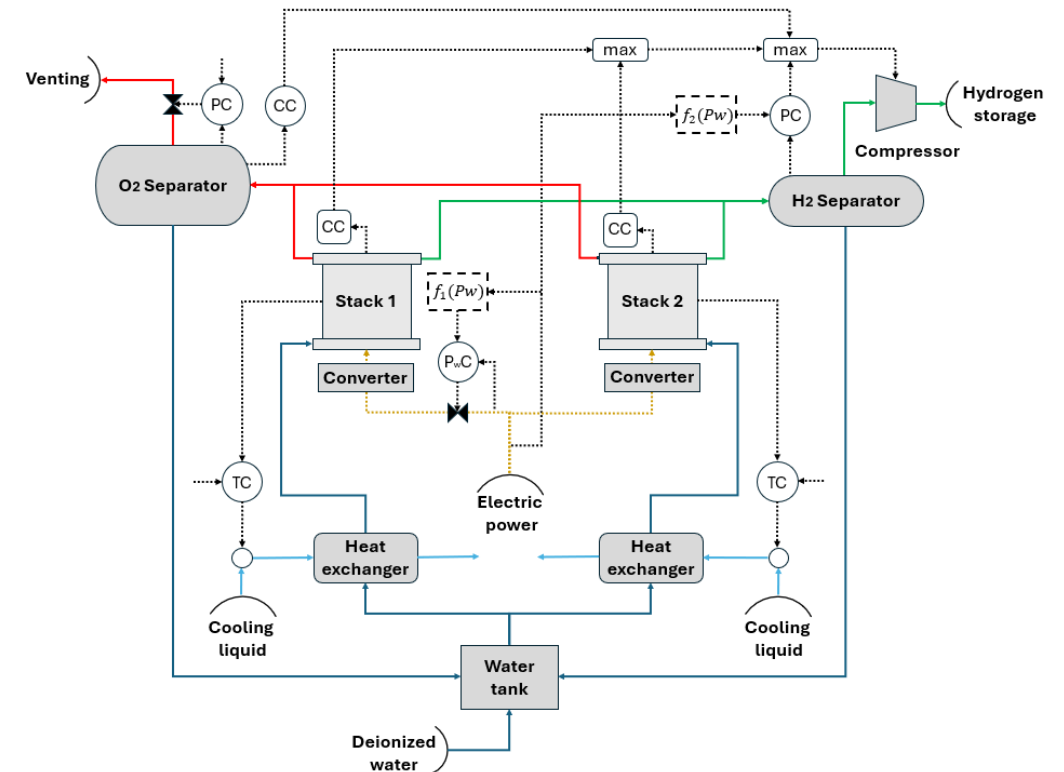
- Selectors added to guard for safety concerns from model mismatch
- HTO and pressure constraints can be met by increasing compression work
- HTO in stacks must be estimated
- HTO in the separator may be measured



Conclusion and Future Work

In this work, we have

- Mapped the optimal operating regime of a two-stack PEM water electrolyzer system.
- Shown that performance differences between stacks fragment the operating space, increasing the number of active constraint regions.
- Showed that HTO constraints in degraded stacks may become a critical limiting factor for hydrogen pressure and power distribution.
- Proposed a simplified control structure for a multi-stack PEM system.



Next steps

- Test the proposed control structure in a dynamic system model.
- Develop state estimators to find the HTO content in the electrolyzer stacks.

Acknowledgements

FME HYDROGENi is financed by its industry partners and the Norwegian government through the Norwegian Research Council's Centres for Environment-friendly Energy Research programme (FMETEKN, project no. 333118)



**Thank you for your
attention!**

